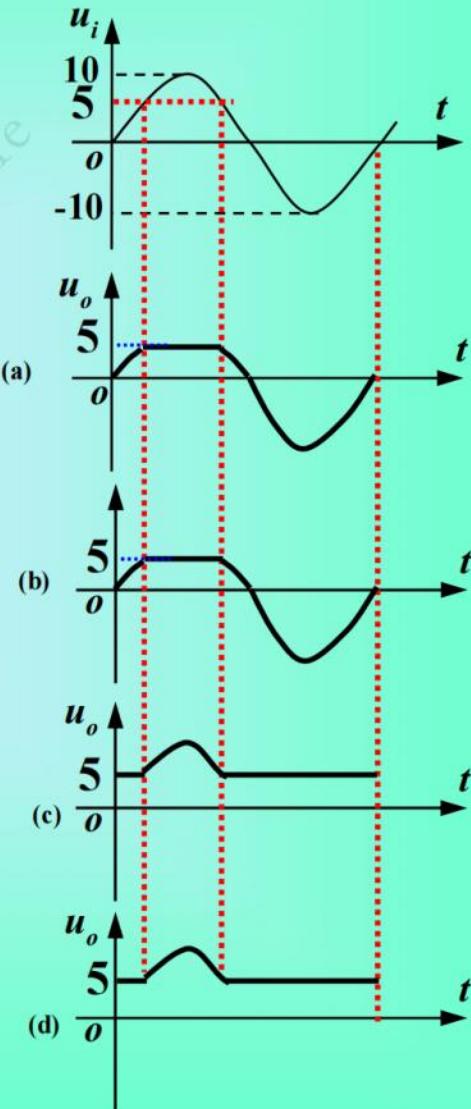
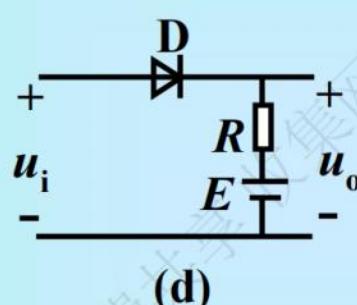
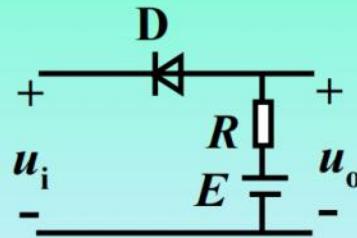
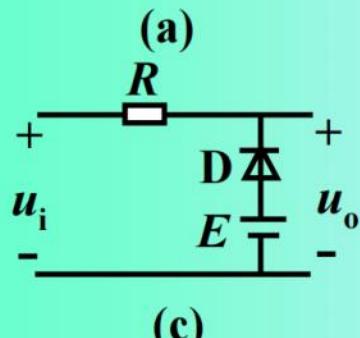
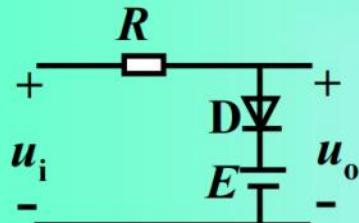
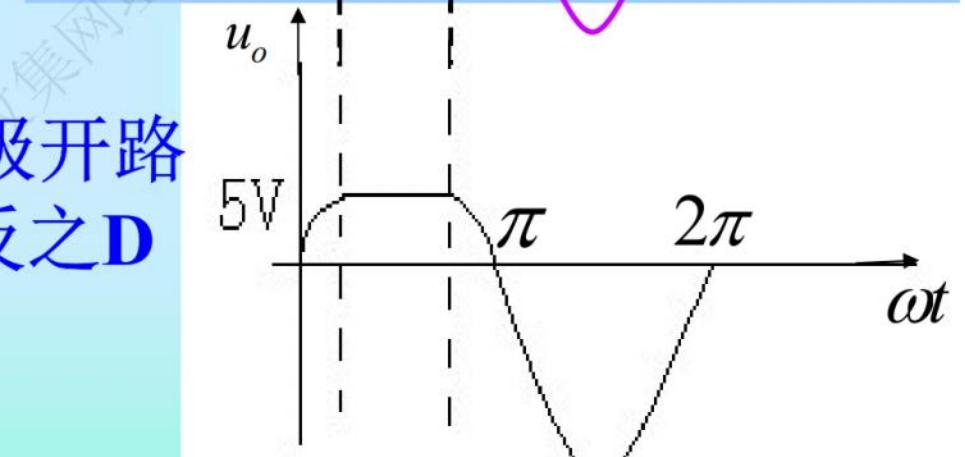
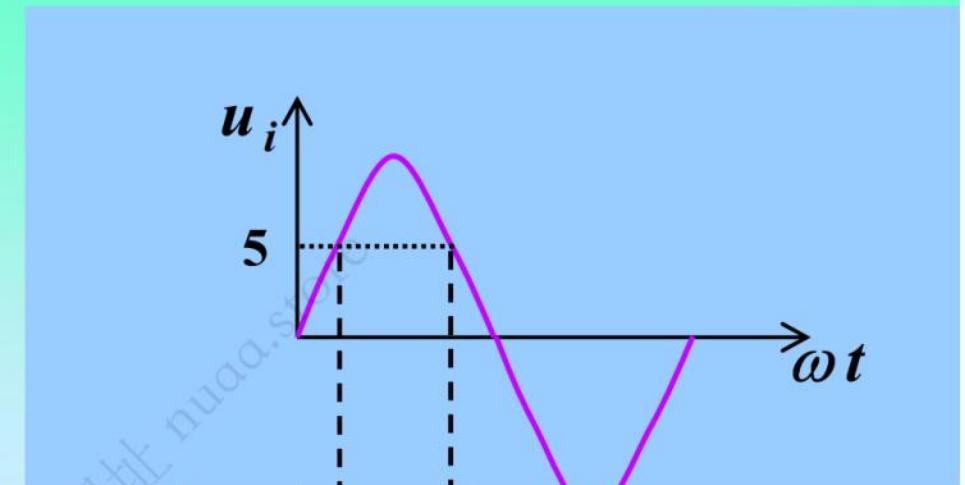
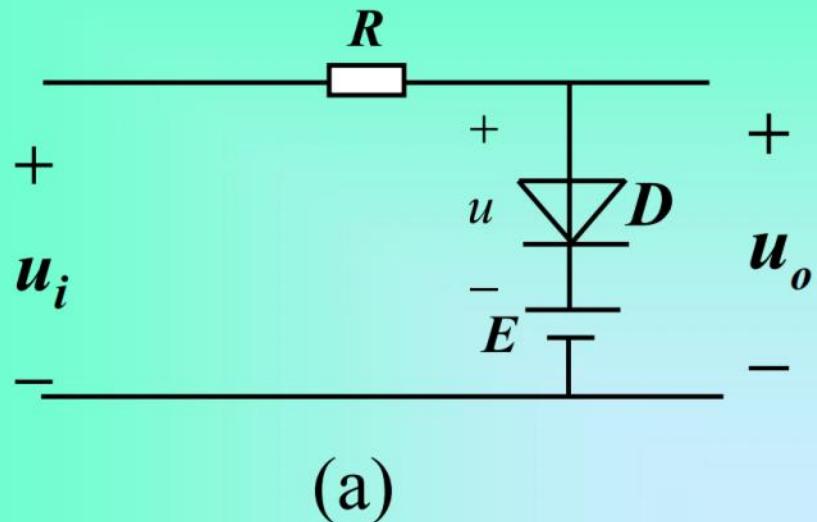


1.1 在图示各电路中,  $E=5V$ , 二极管的正向压降可忽略不计, 试分别画出输出电压 $u_o$ 的波形。



1.1:



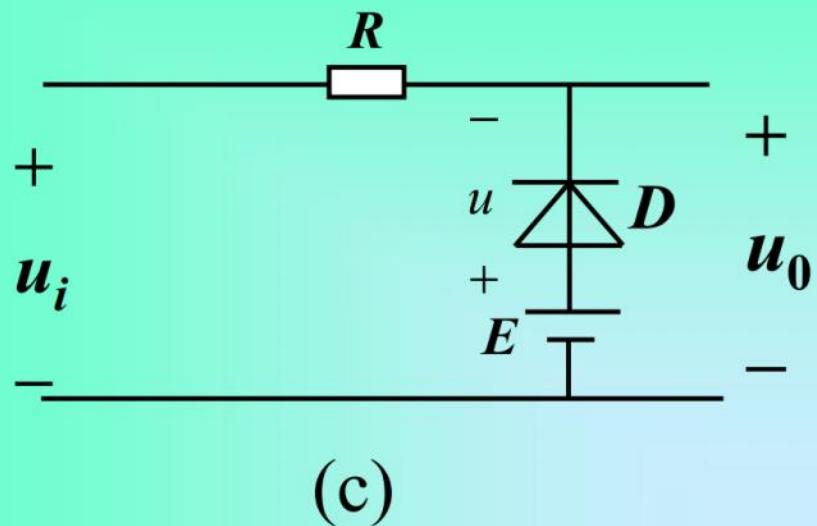
解: 将D开路, 求其阳、阴两极开路电压, 若>0, 则D导通; 反之D截止。

$$u = u_i - 5$$

若<sub>i</sub><5V, <0, D截止, <sub>0</sub>=<sub>i</sub>

若<sub>i</sub>>5V, >0, D导通, <sub>0</sub>=5V

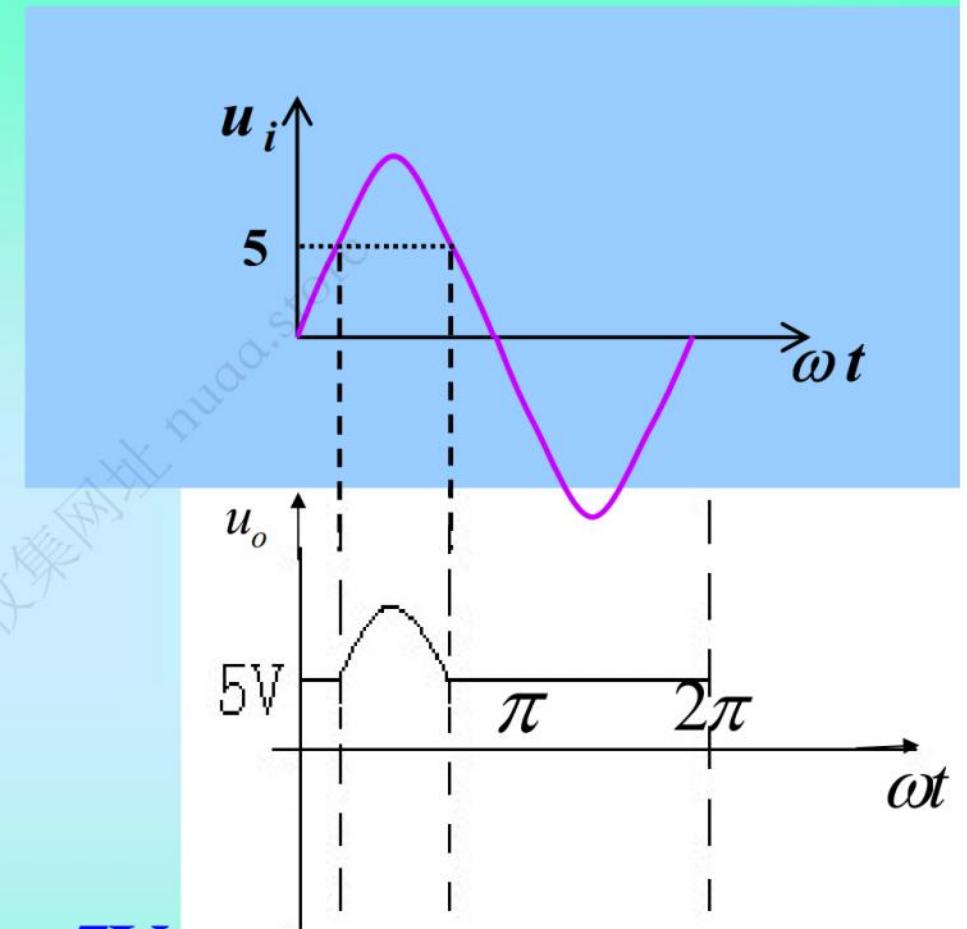
1. 1:



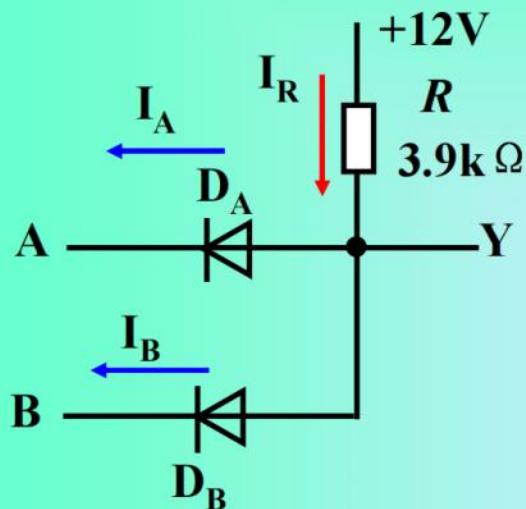
$$u = 5 - u_i$$

若  $u_i < 5V, u > 0, D$  导通,  $u_0 = 5V$

若  $u_i > 5V, u < 0, D$  截止,  $u_0 = u_i$



1.2 试求输出端Y的电位 $V_Y$ 及各元件 ( $R$ 、  $D_A$ 、  $D_B$ ) 中通过的电流：  
 (1)  $V_A = V_B = 0V$ ; (2)  $V_A = +3V$ ,  $V_B = 0V$ ; (3)  $V_A = V_B = 3V$ 。



(1)  $D_A$ 通,  $D_B$ 通,  $V_Y = 0V$ ;

$$I_R = 2 I_A = 2 I_B = 12/3.9 = 3.08mA$$

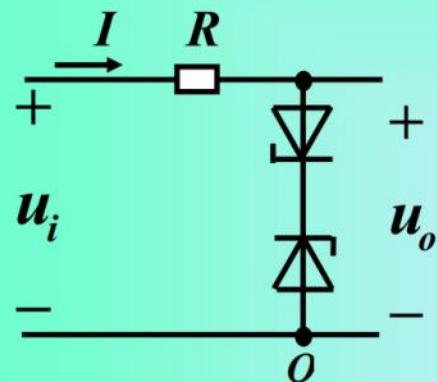
(2)  $D_B$ 通,  $D_A$ 止,  $V_Y = 0V$ ;

$$I_R = I_B = 12/3.9 = 3.08mA$$

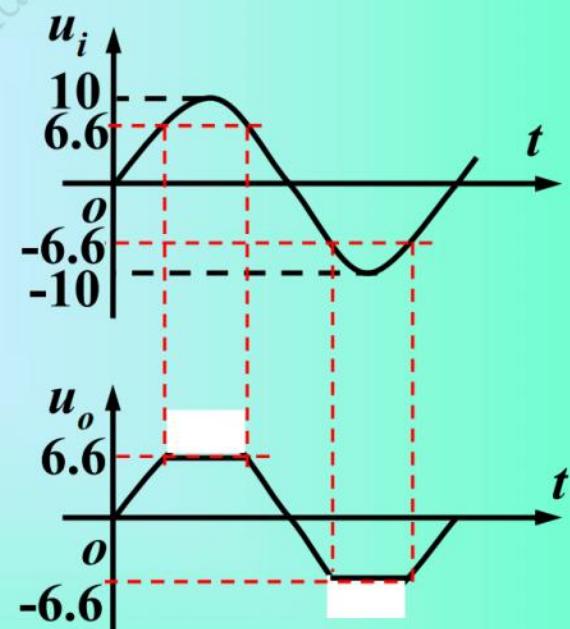
(3)  $D_A$ 通,  $D_B$ 通,  $V_Y = 3V$ ;

$$I_R = 2 I_A = 2 I_B = 9/3.9 = 2.3mA$$

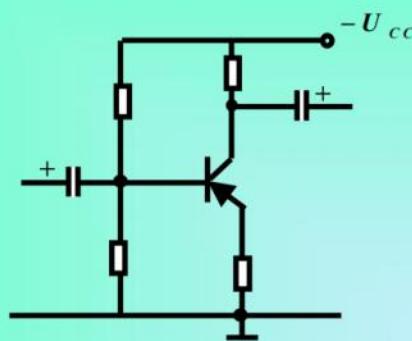
1.3 图示电路中，若稳压管的稳定电压 $U_Z$ 都是6V，正向导通压降均为0.6V，试画出输出电压 $u_o$ 的波形。



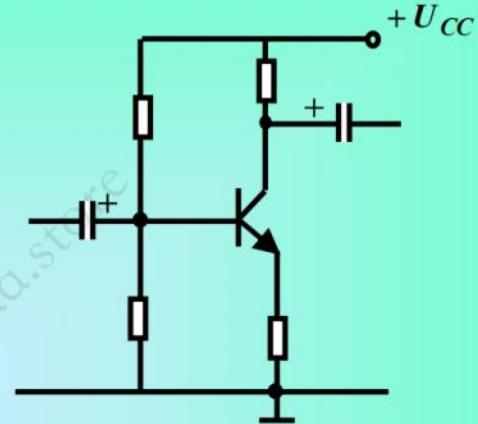
$$u_i = 10 \sin \omega t \text{V}$$



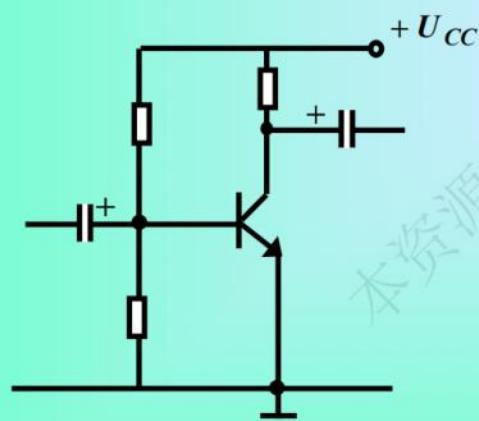
## 2.3 试判断图示各个电路能不能放大交流信号？为什么？



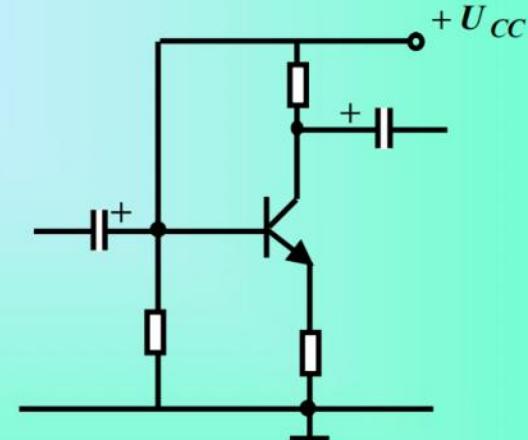
可以，偏置正确



可以，偏置正确

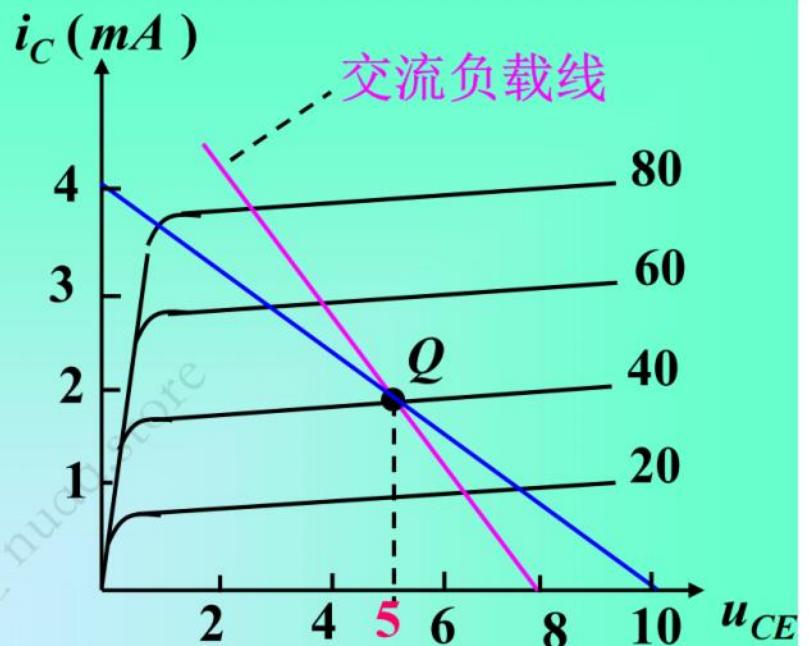
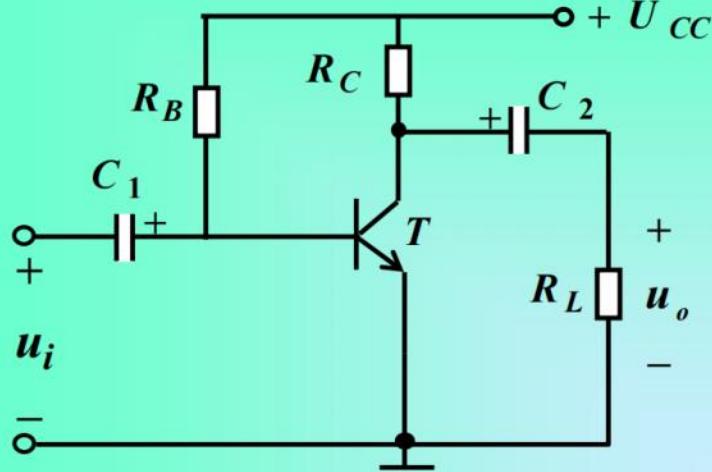


可以



不可以，输入端短路

## 2.4



(1) 从直流负载线可以看出,  $U_{CC}=10V$

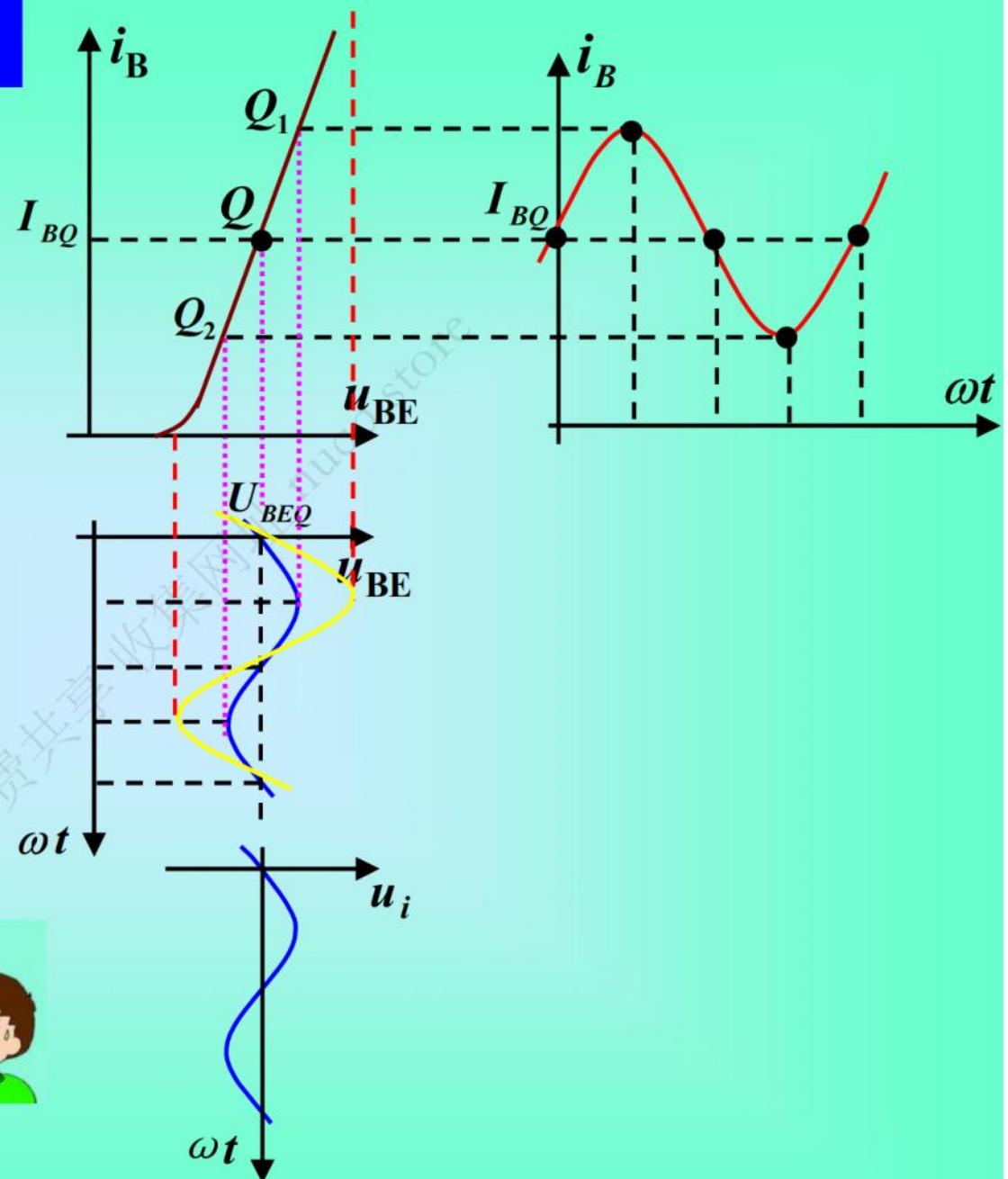
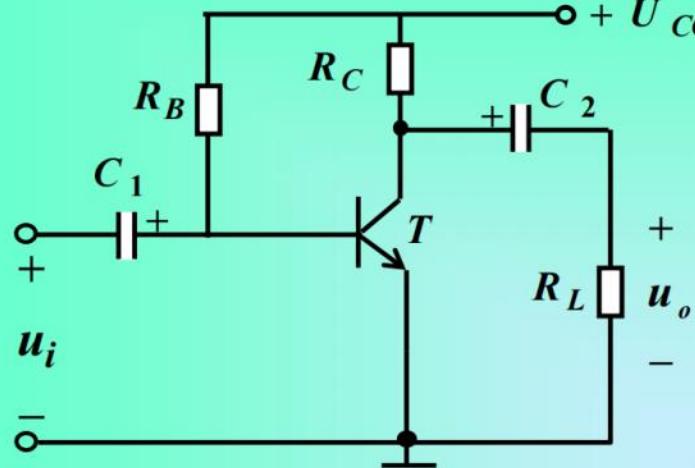
$$\tan \alpha = -\frac{1}{R_C} = -\frac{2}{5} \text{ 因此 } R_C = 2.5K\Omega$$

Q点对应的  $I_{CQ}=2mA$ ,  $I_{BQ}=40\mu A$ ,  $U_{CEQ}=5V$

$$I_B = \frac{U_{CC} - U_{BE}}{R_B} \approx \frac{U_{CC}}{R_B} = \frac{10}{R_B} = 40\mu A \Rightarrow R_B = 250k\Omega$$

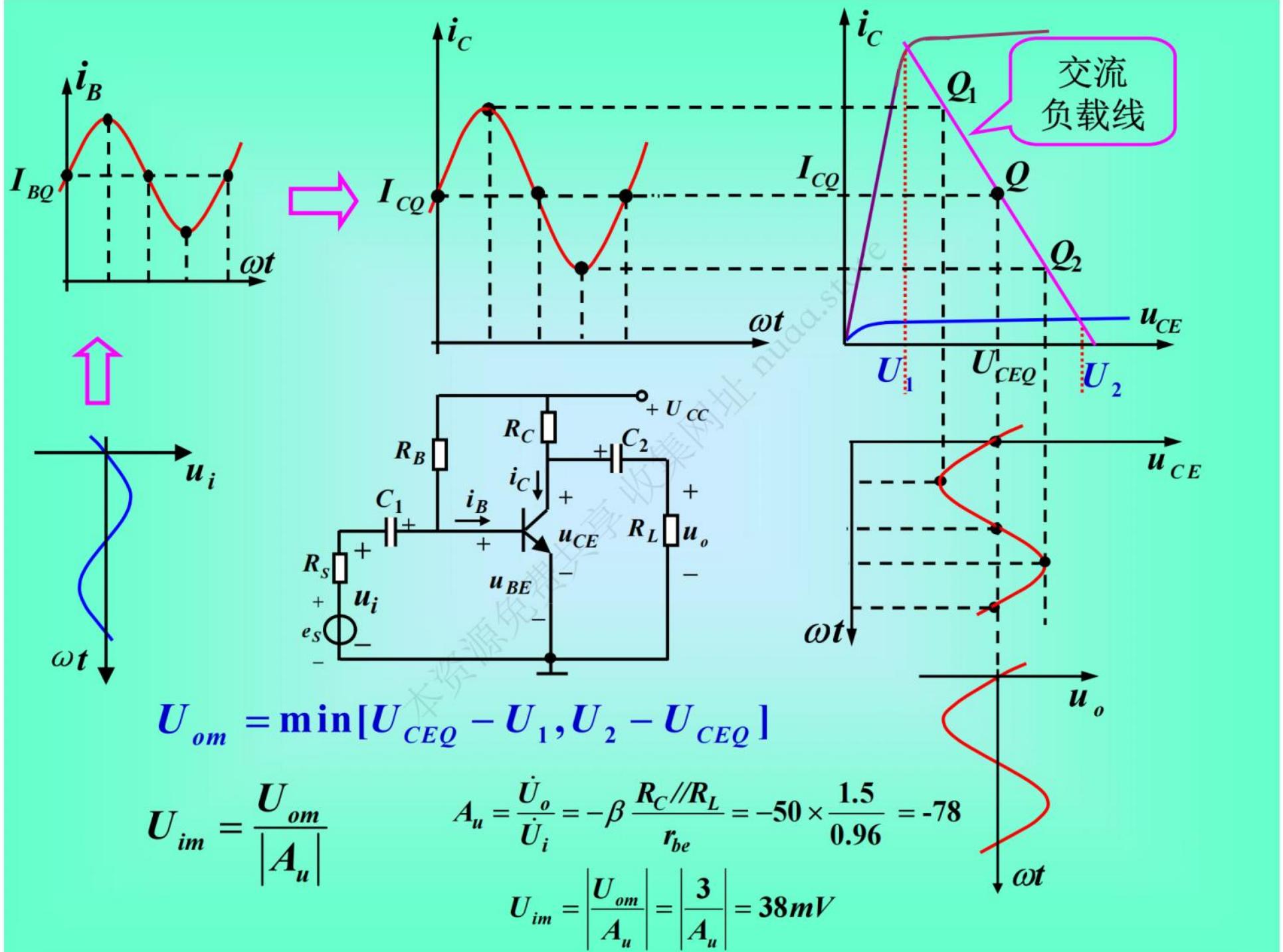
$$\text{交流负载线斜率: } -\frac{1}{R_L // R_C} = -\frac{2}{8-5} = -\frac{2}{3} \Rightarrow R_L = 3.75k\Omega$$

## 2) 输入过大引起的失真



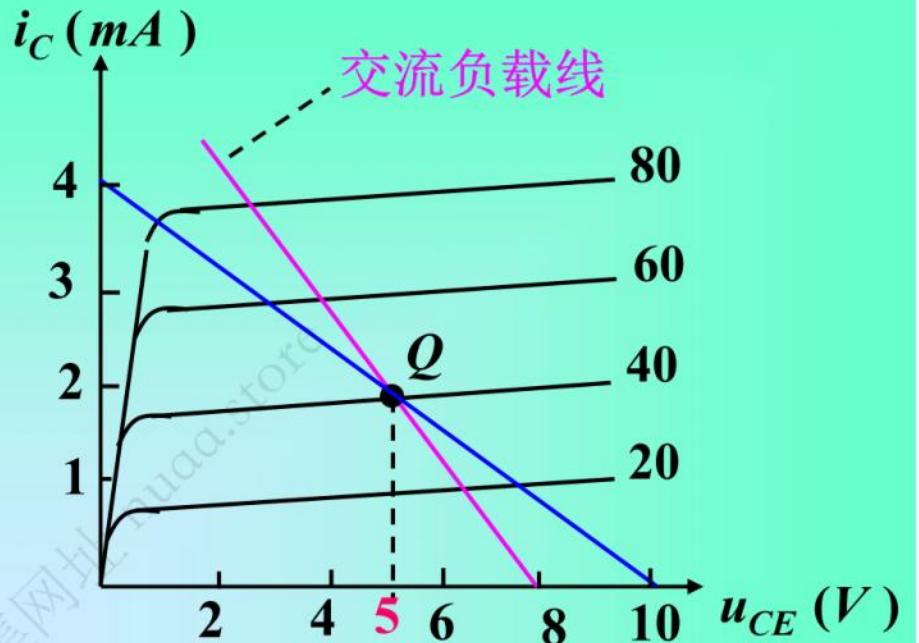
$$U_{im} = U_{BEQ} - U_T$$

输入曲线仅考虑截止失真，还要在输出曲线中考虑饱和失真



(3) 输出首先出现什么失真?

首先出现截止失真，减小  $R_B$

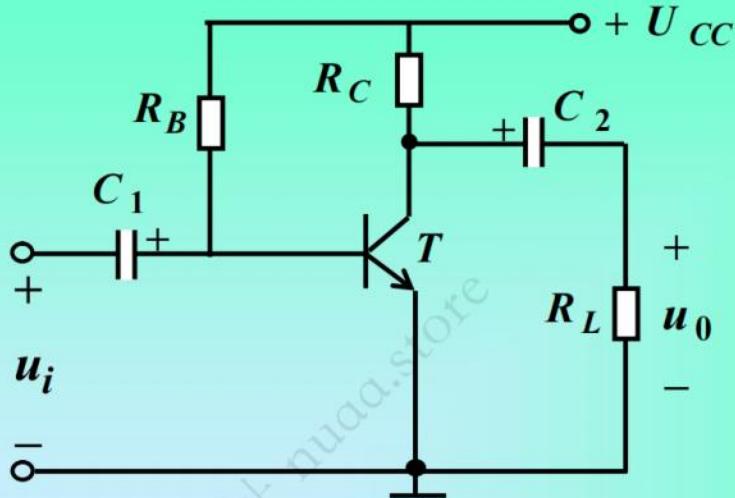


(4) 增大  $R_L$ ，对直流负载线无影响，

但使交流负载线的斜率绝对值减小，变的更平坦

交流负载线的  $\tan \alpha' = -\frac{1}{R_L}$

(5)  $\beta$ 减小一半



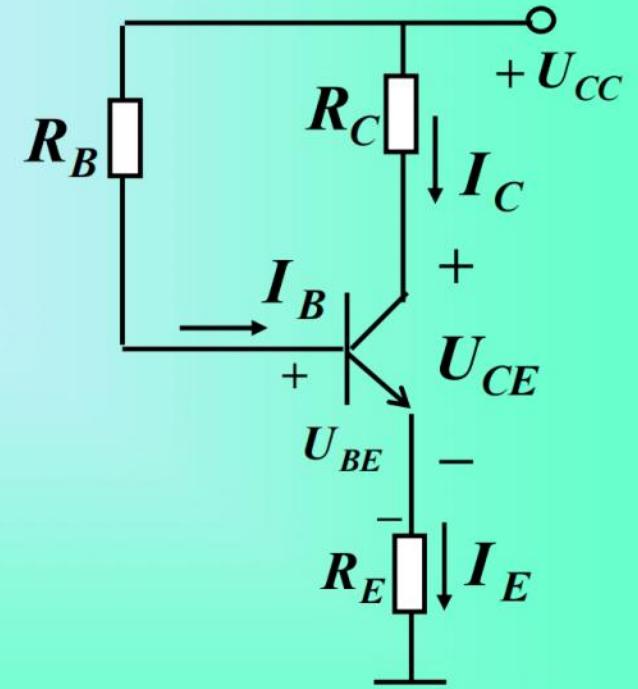
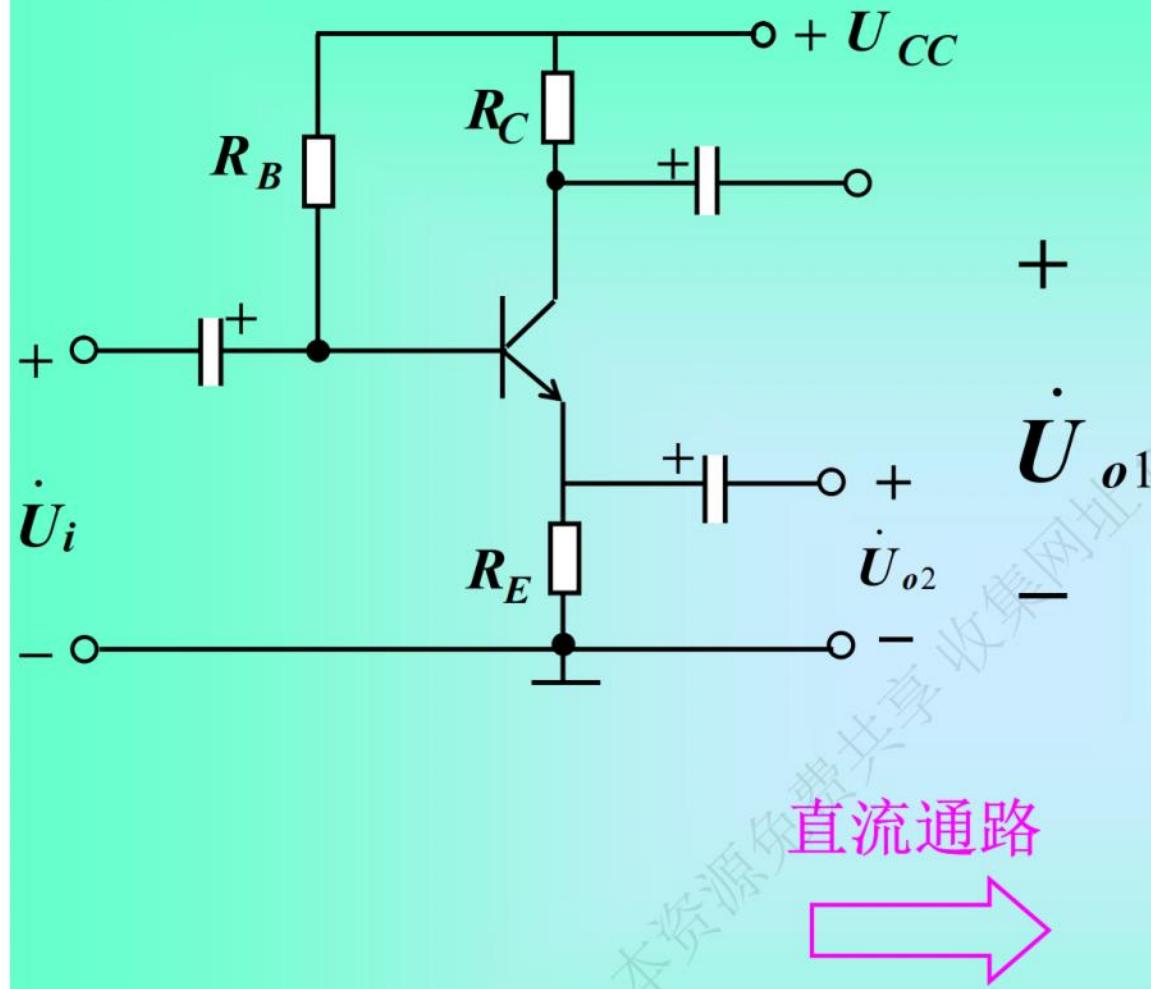
$$I_B = \frac{U_C - U_{BE}}{R_B} \approx \frac{U_C}{R_B} = \frac{10}{R_B} = 40 \mu A$$

$I_C = \beta I_B$        $I_C$ 降为原来的一半       $U_{CE} = U_{CC} - I_C R_C$  变大

$$r_{be} \approx 300 + (1 + \beta) \frac{26(mV)}{I_E(mA)} = 300 + \frac{26(mV)}{I_B(mA)} \quad r_{be} \text{ 不变}$$

$$A_u = \frac{\dot{U}_o}{\dot{U}_i} = -\beta \frac{R_C // R_L}{r_{be}} \text{ 减小一半}$$

2.5

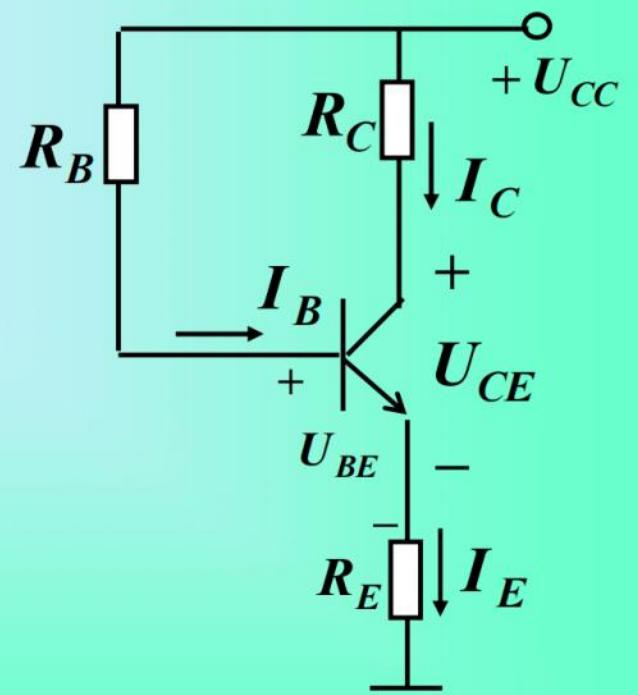


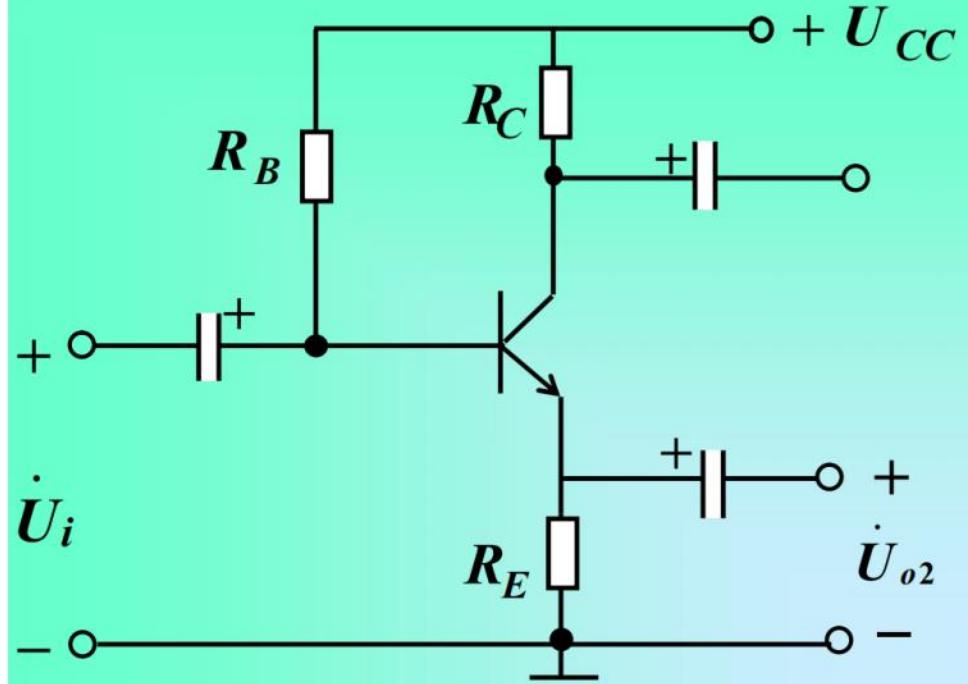
$$U_{CC} = R_B I_B + U_{BE} + (1 + \beta) R_E I_B$$

$$I_B = \frac{U_{CC} - U_{BE}}{R_B + (1 + \beta) R_E} \approx 30 \mu A$$

$$I_E = (1 + \beta) I_B \approx 1.5 mA$$

$$r_{be} \approx 300 + (1 + \beta) \frac{26(mV)}{I_E(mA)} = 1.18 k\Omega$$

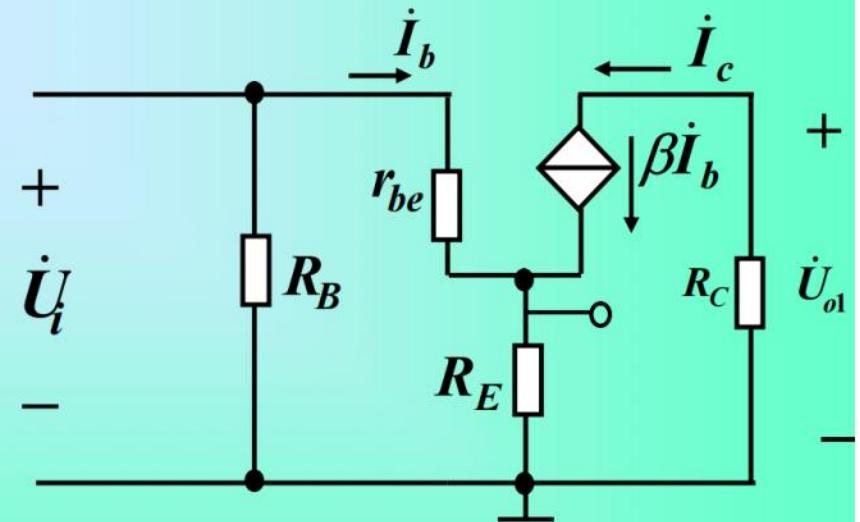


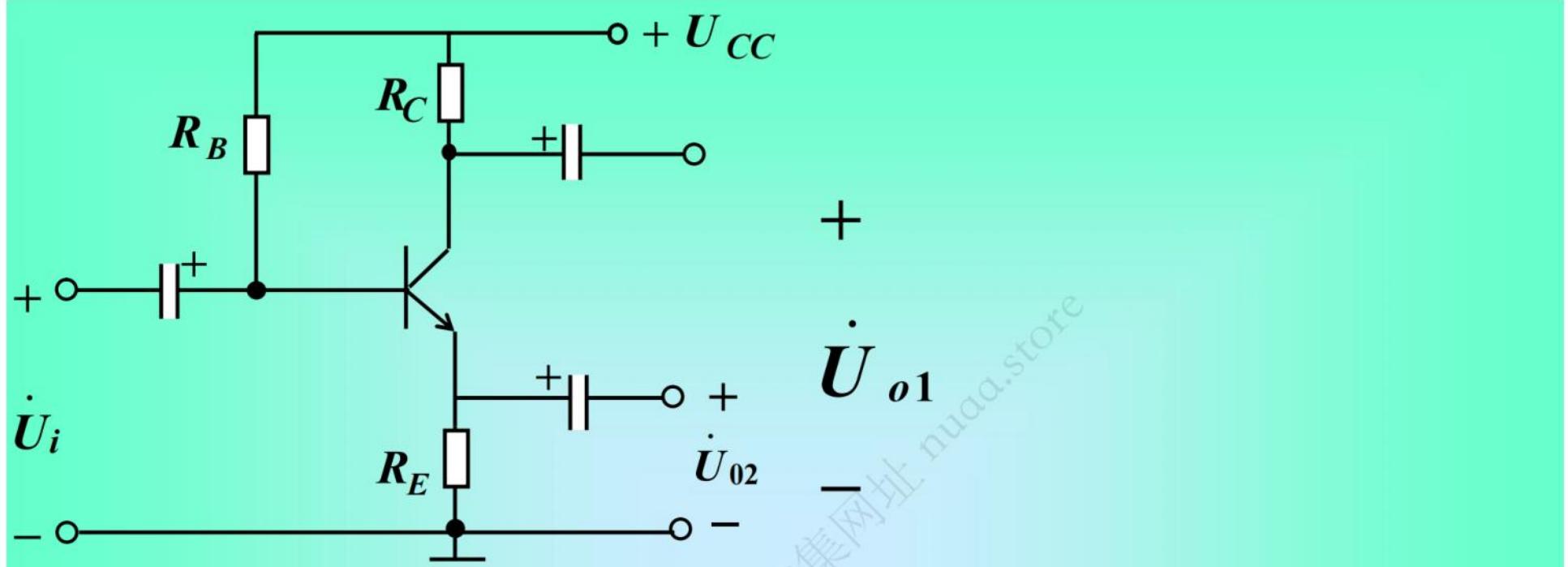


$$\dot{U}_{o1} = -\beta \dot{I}_b R_C$$

$$\dot{U}_i = \dot{I}_b r_{be} + (1 + \beta) \dot{I}_b R_E$$

$$A_{u1} = \frac{\dot{U}_{o1}}{\dot{U}_i} = -\frac{\beta R_C}{r_{be} + (1 + \beta) R_E} = -0.97$$

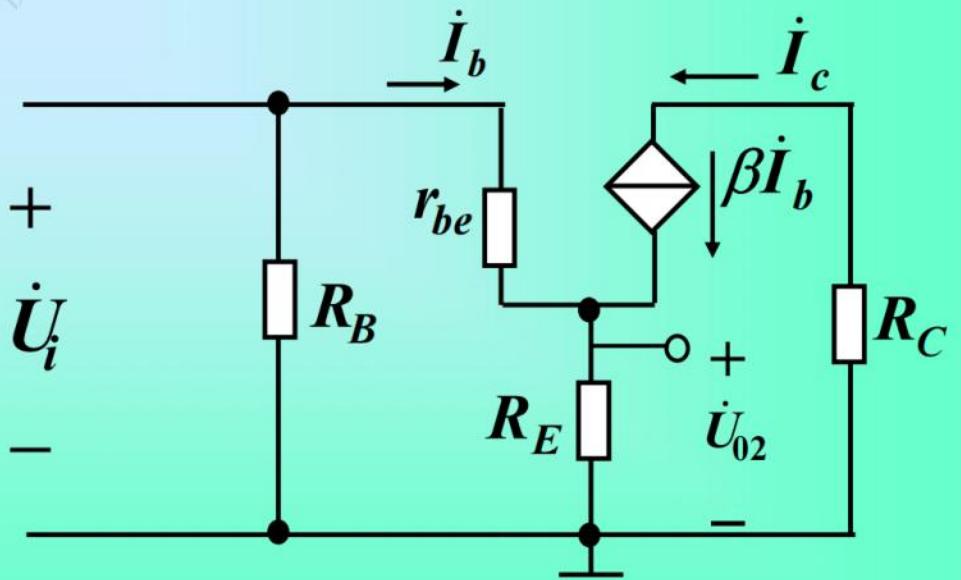




$$\dot{U}_{o2} = (1 + \beta) \dot{I}_b R_E$$

$$\dot{U}_i = \dot{I}_b r_{be} + (1 + \beta) \dot{I}_b R_E$$

$$A_{u2} = \frac{\dot{U}_{o2}}{\dot{U}_i} = \frac{(1 + \beta) R_E}{r_{be} + (1 + \beta) R_E} = 0.99$$



求输出电阻

$$r_{o1} = R_C$$

$$r_{o2} = \frac{\dot{U}}{\dot{I}}$$

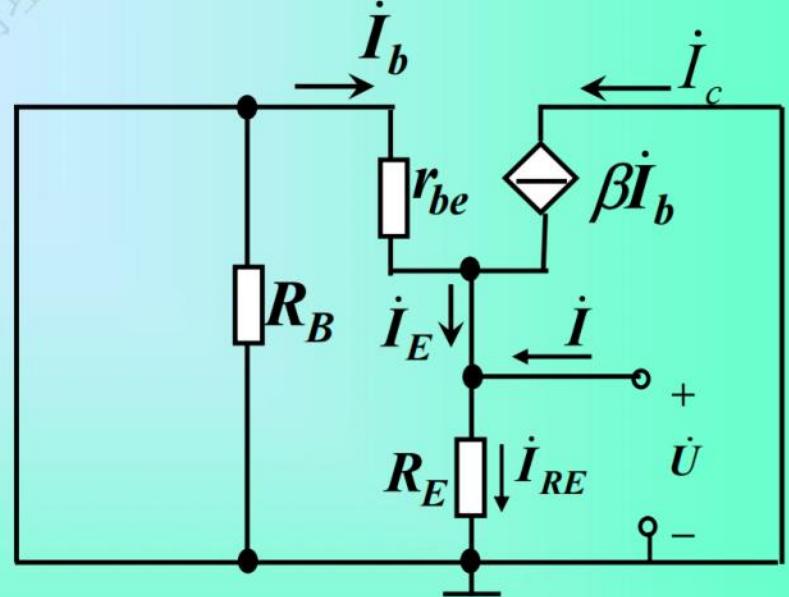
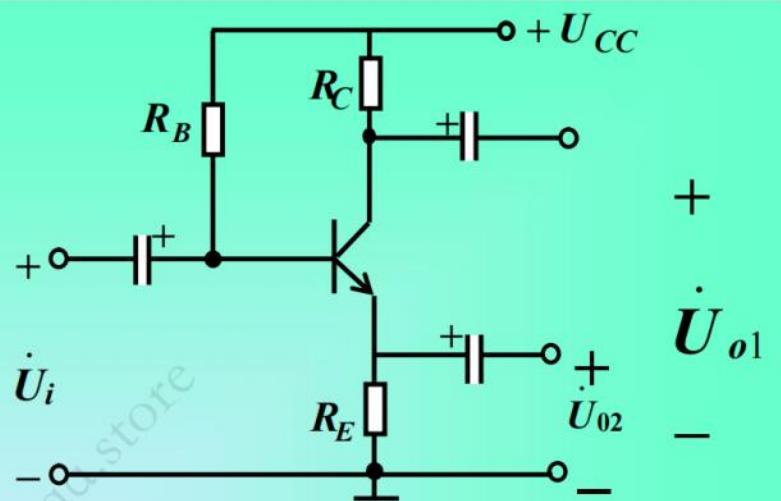
$$\dot{I} = \dot{I}_E + \dot{I}_{RE} = (1 + \beta) \dot{I}_b + \dot{I}_{RE}$$

$$\dot{U} = -\dot{I}_b r_{be} \quad \rightarrow \quad \dot{I}_b = -\frac{\dot{U}}{r_{be}}$$

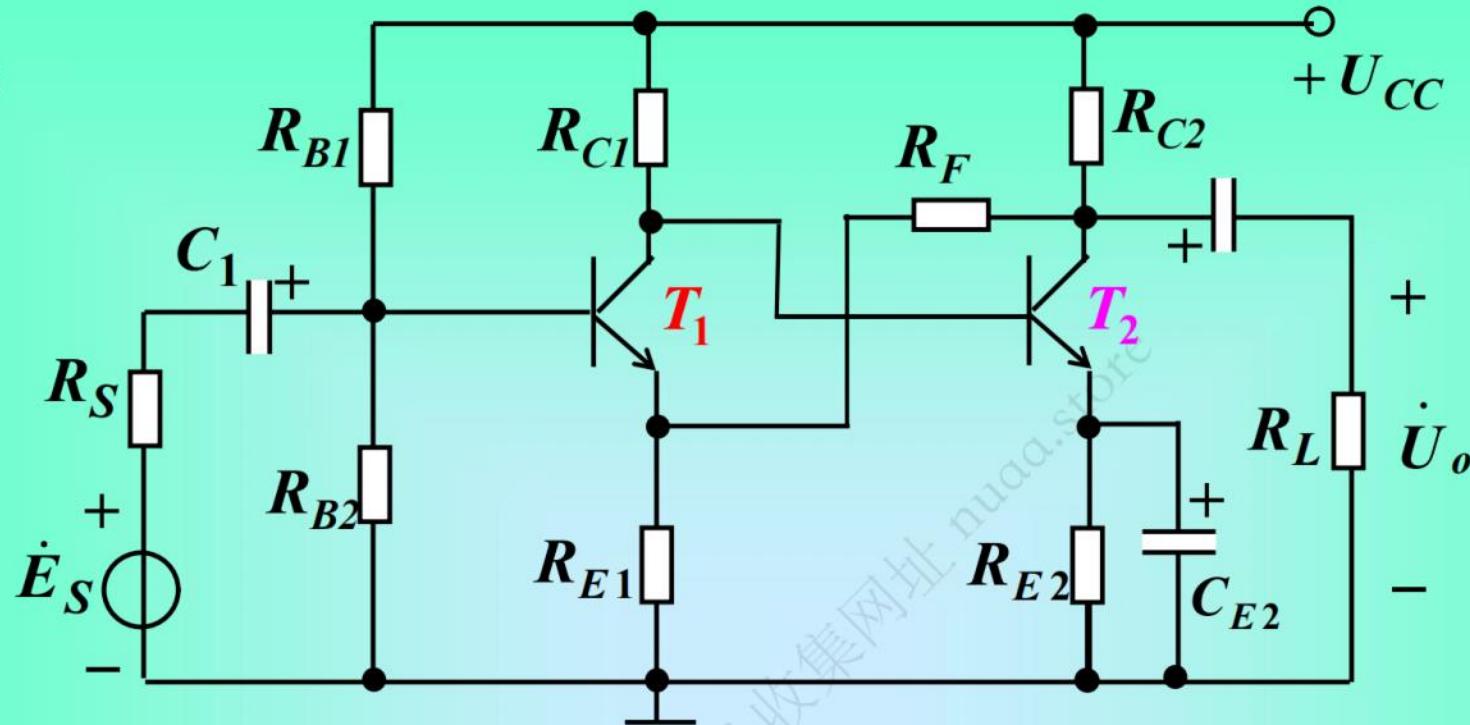
$$\dot{I}_{RE} = \frac{\dot{U}}{R_E}$$

$$\dot{I} = \frac{\dot{U}}{R_E} + (1 + \beta) \frac{\dot{U}}{r_{be}}$$

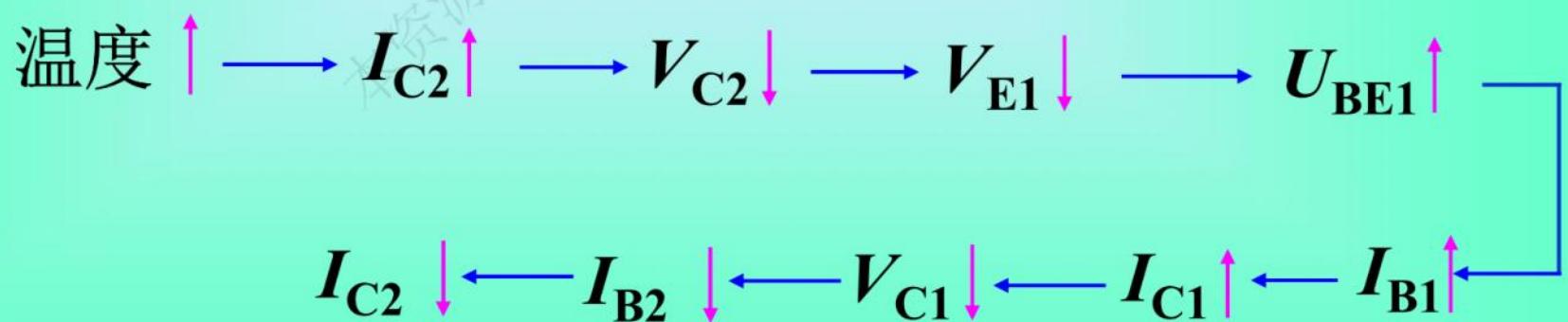
$$r_{o2} = \frac{\dot{U}}{\dot{I}} \approx \frac{r_{be}}{1 + \beta} = 23\Omega$$

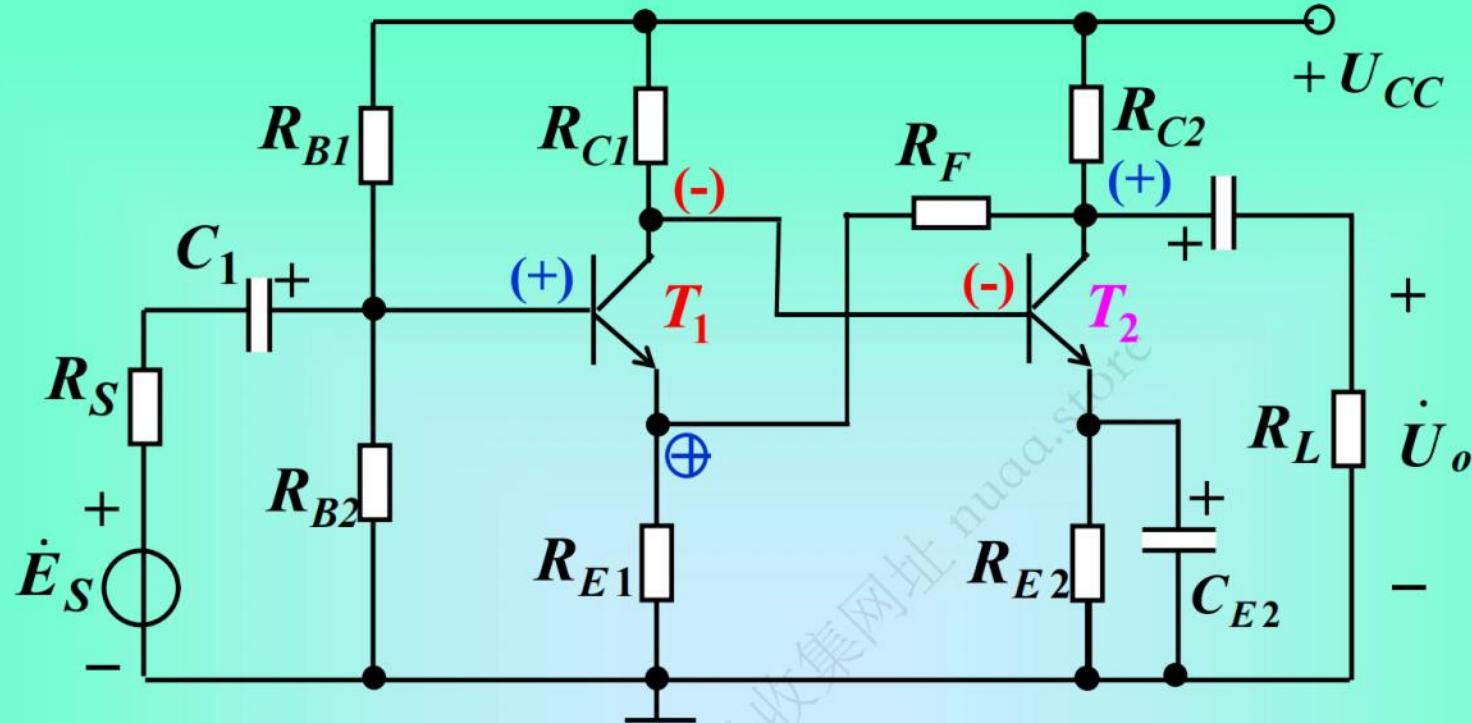


2.6



1、直流负反馈:  $R_{E1}$ 、 $R_{E2}$ 、 $R_F$





## 2、交流负反馈

$R_{E1}$ : 电流串联负反馈

$R_F$ : 电压串联负反馈

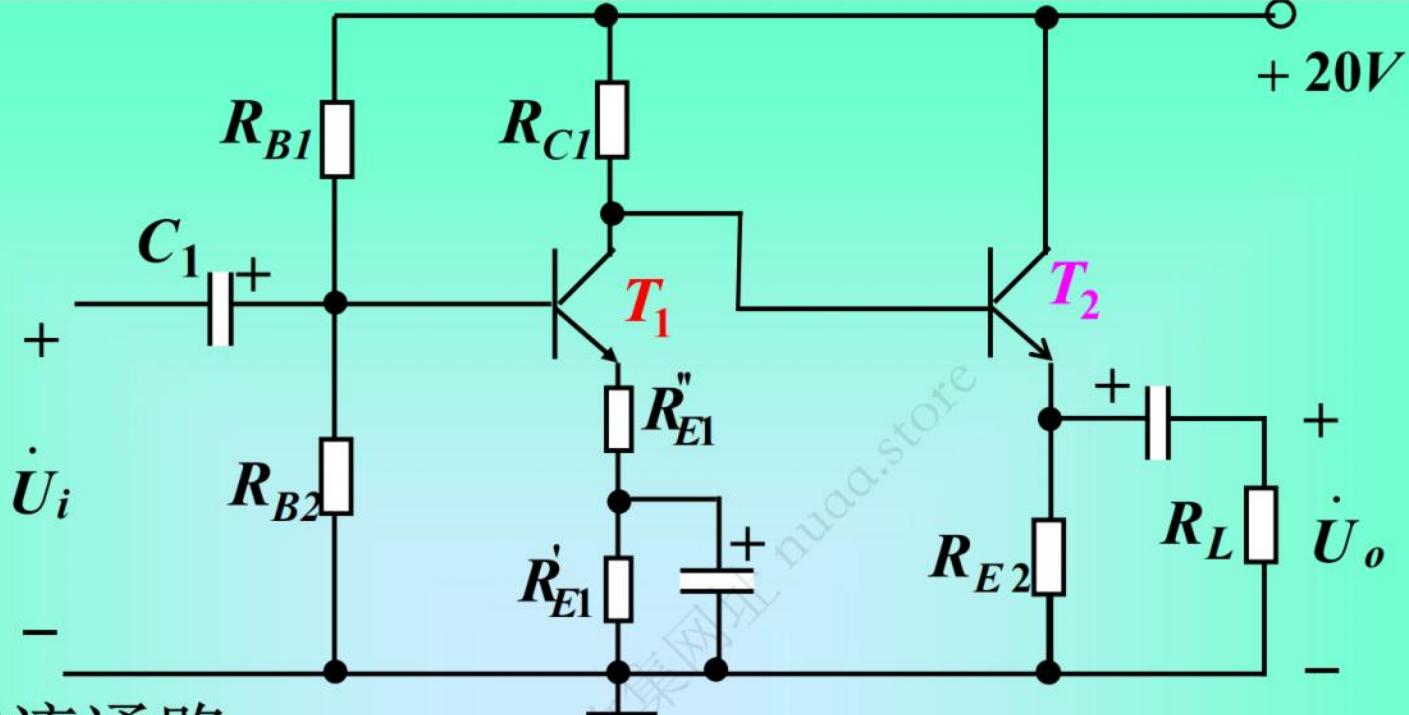
3、如 $R_F$ 不接在T2的集电极，而接在 $C_2$ 与 $R_L$ 之间，两者有何不同？

将只有交流负反馈

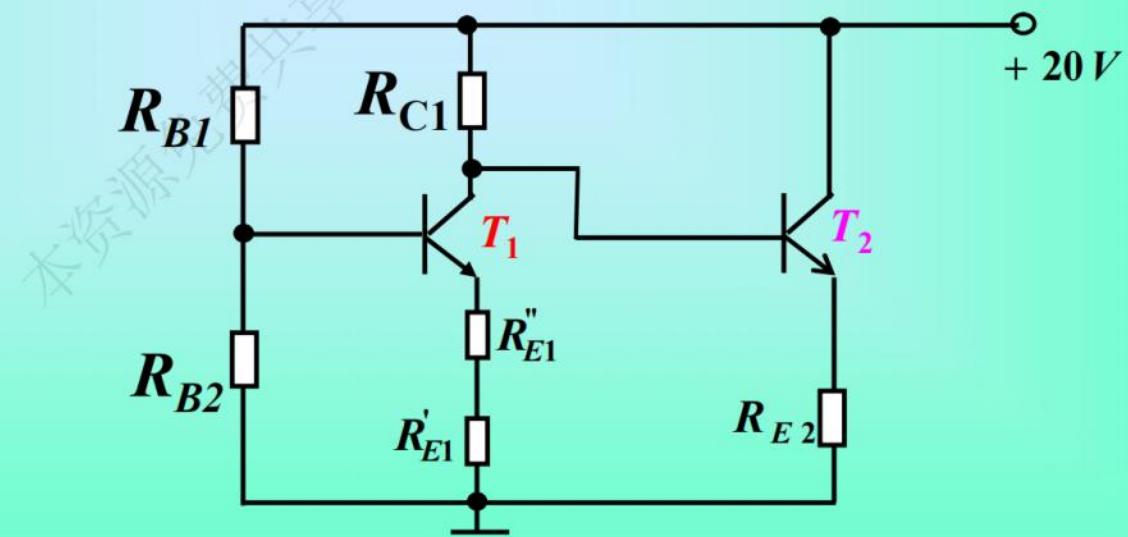
4、如果 $R_F$ 的另一端不是接在T1的发射极，而是接在它的基极，则有何不同？是否会变成正反馈？

会变成电压并联正反馈

2.7

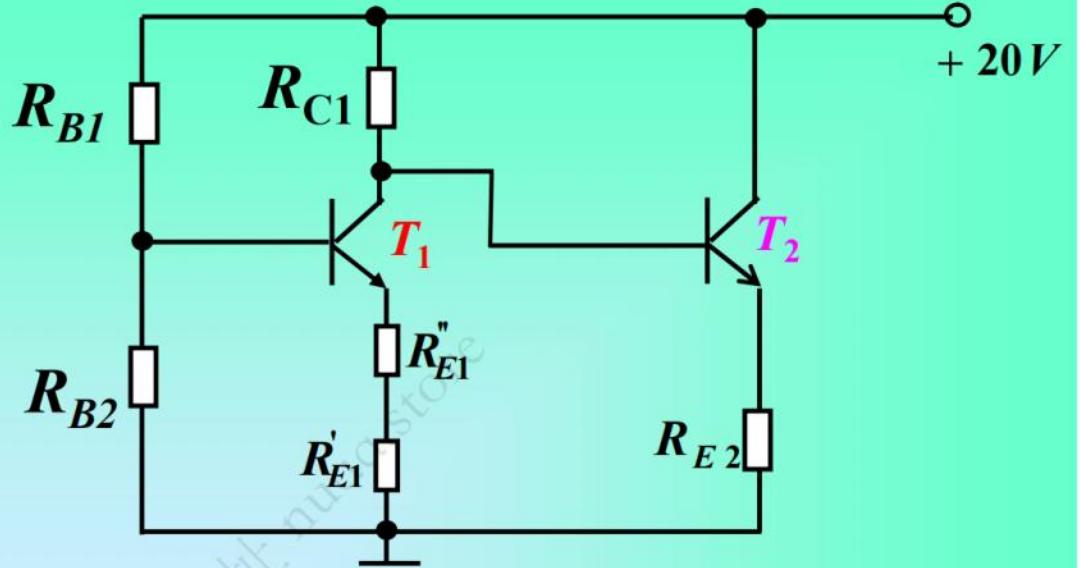


(1) 画直流通路



第一级：

$$V_{B1} \approx \frac{R_{B2}}{R_{B1} + R_{B2}} \times 20 = 4V$$



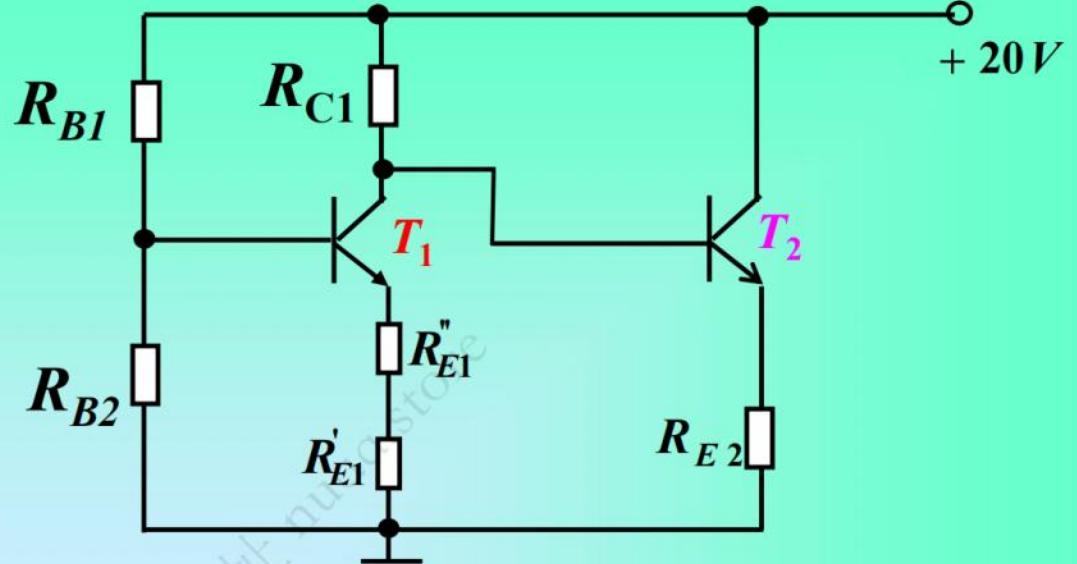
$$I_{C1} \approx I_{E1} = \frac{V_{B1} - U_{BE1}}{R_{E1}} = \frac{4 - 0.6}{3.39} = 1mA$$

$$I_{B1} = \frac{I_{C1}}{\beta_1} = 25\mu A$$

$$U_{CE1} \approx U_{CC} - I_{C1}(R_{C1} + R'_E1 + R''_E1) = 20 - 13.4 = 6.6V$$

$$r_{be1} = 300 + (1 + \beta_1) \frac{26}{I_{E1}} = 1.34k\Omega$$

第二级：

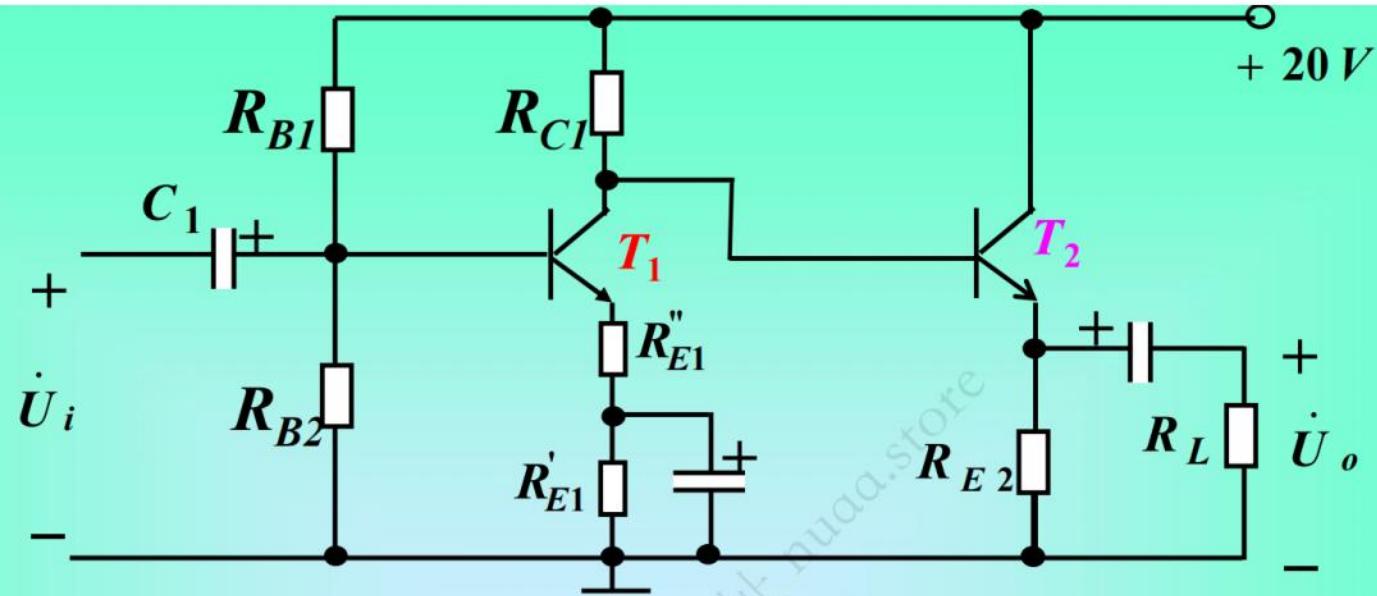


$$V_{B2} = V_{C1} = 20 - I_C R_{C1} = 10V$$

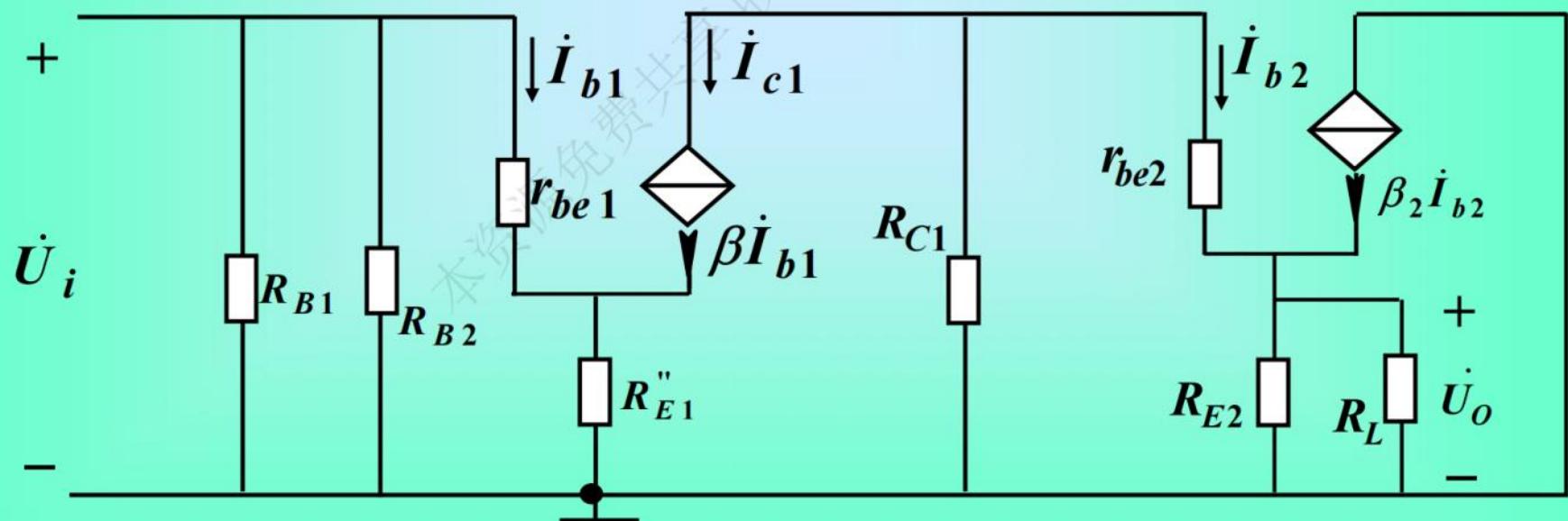
$$I_{C2} \approx I_{E2} = \frac{V_{B2} - U_{BE2}}{R_{E2}} = \frac{10 - 0.6}{5.1} = 1.84mA \quad I_{B2} = \frac{I_{C2}}{\beta_2} = 46\mu A$$

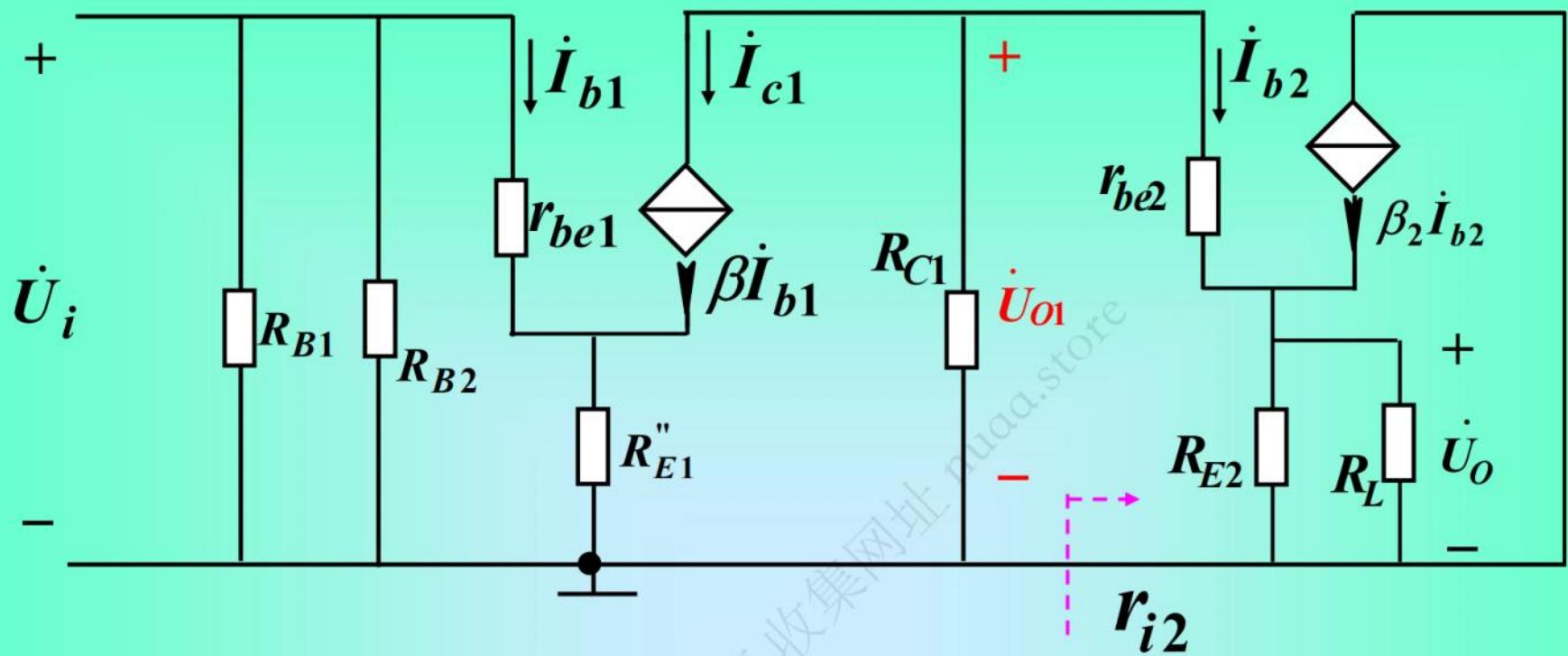
$$U_{CE2} = U_{CC} - I_{C2} R_{E2} = 10.6V$$

$$r_{be2} = 300 + (1 + \beta_2) \frac{26}{I_{E2}} = 0.879k\Omega$$



(2) 求交流参数

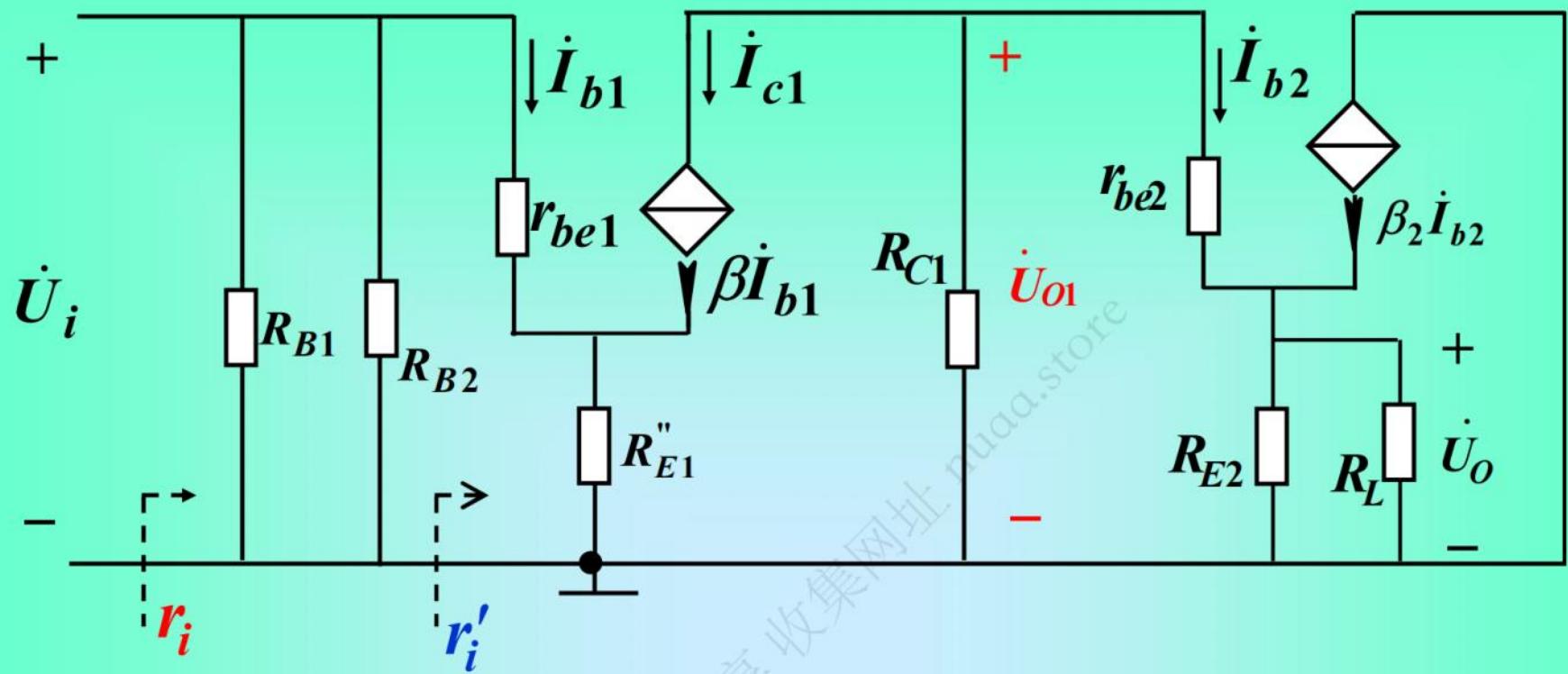




$$A_{u1} = \frac{\dot{U}_{o1}}{\dot{U}_i} = -\beta_1 \frac{R_{C1} // r_{i2}}{r_{be1} + (1 + \beta_1) R''_E} = -\beta_1 \frac{R_{C1} // [r_{be2} + (1 + \beta_2) R_{E2} // R_L]}{r_{be1} + (1 + \beta_1) R''_E} = -21$$

$$A_{u2} = \frac{\dot{U}_o}{\dot{U}_{o1}} = \frac{(1 + \beta_2) R_{E2} // R_L}{r_{be2} + (1 + \beta_2) R_{E2} // R_L} = 0.99$$

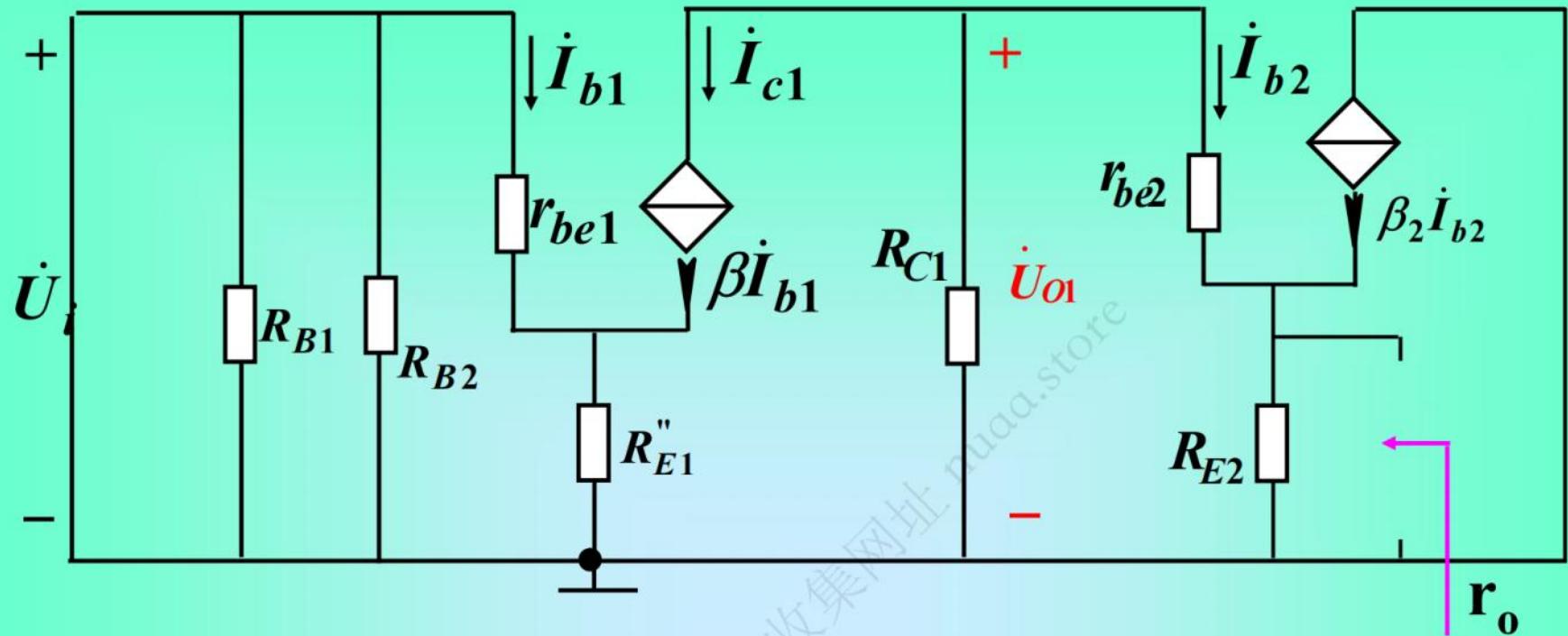
$$A_u = \frac{\dot{U}_o}{\dot{U}_i} = A_{u1} A_{u2} = -21$$



求输入电阻

$$r_i = \frac{\dot{U}_i}{\dot{I}_i} = R_{B1} // R_{B2} // r'_i$$

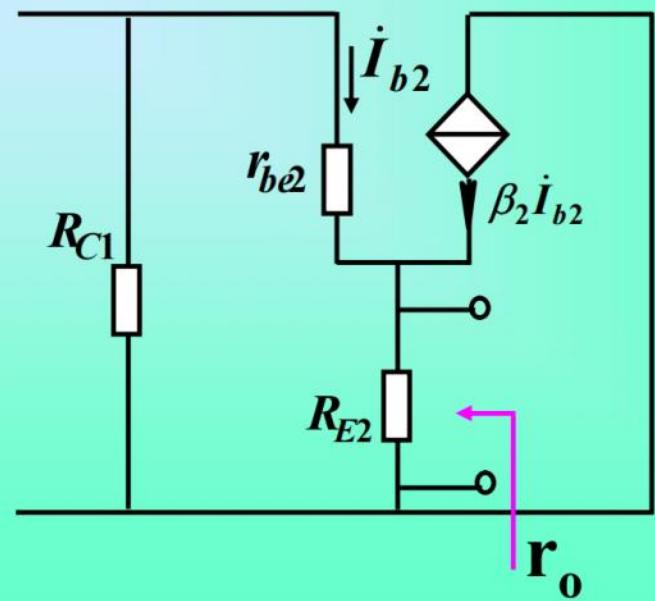
$$\text{而 } r'_i = \frac{\dot{U}_i}{\dot{I}_b} = r_{be1} + (1 + \beta_1) R_E''$$



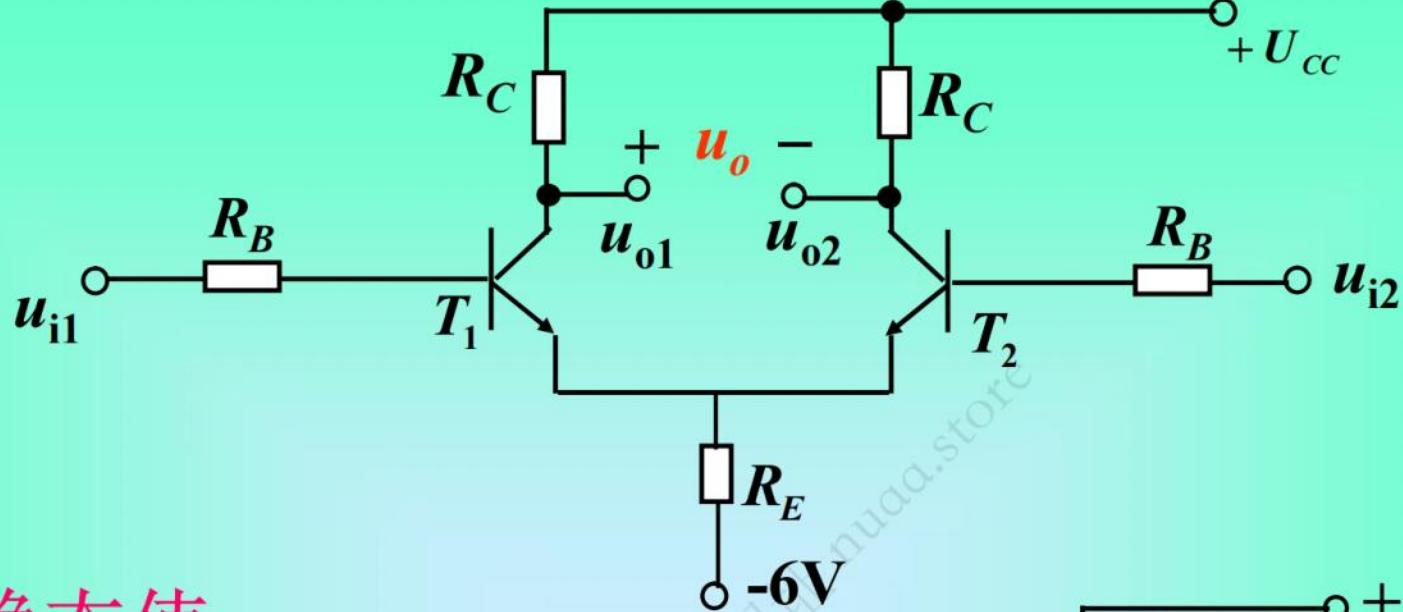
求输出电阻

$$r_o = \frac{R_{E2}(R_{C1} + r_{be2})}{(1 + \beta) R_{E2} + R_{C1} + r_{be2}}$$

$$\approx \frac{R_{C1} + r_{be2}}{(1 + \beta)}$$



2.9



(1) 求静态值

$$I_B \cdot R_B + U_{BE} + 2I_E \cdot R_E = 6$$

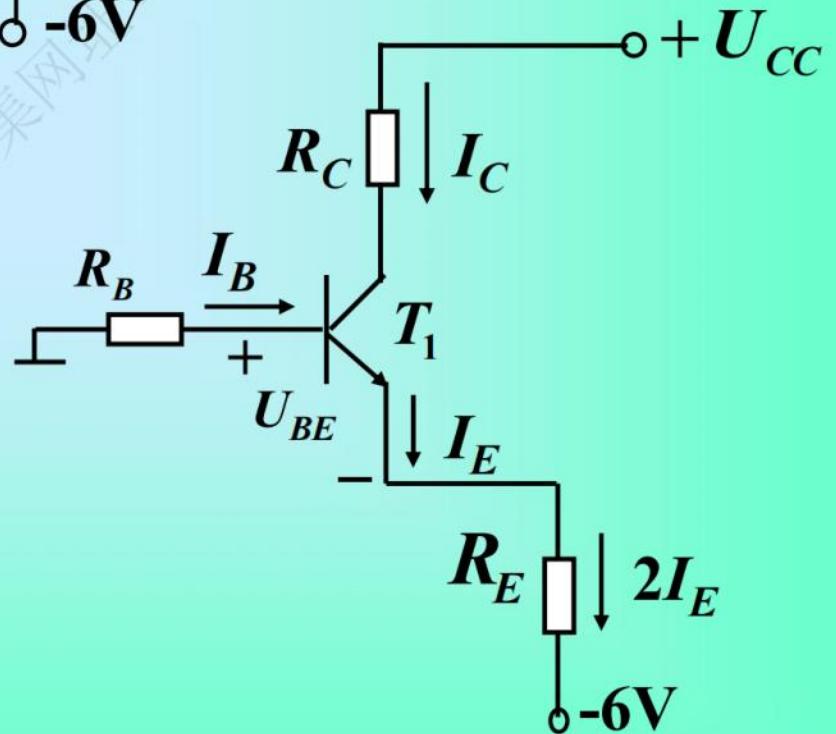
$$I_B = \frac{E_E - U_{BE}}{R_B + 2(1 + \beta)R_E} = 0.01mA$$

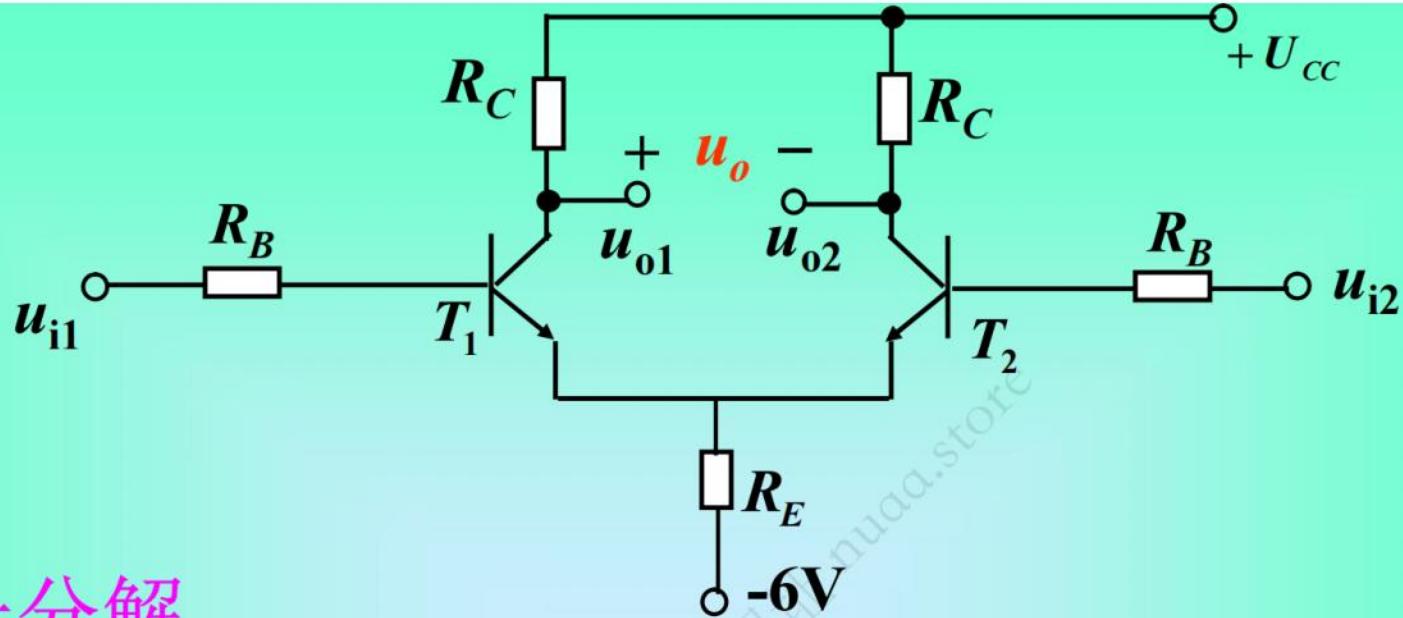
$$I_C = \beta I_B = 0.5mA \approx I_E$$

$$V_B = -I_B R_B = -0.1V$$

$$V_C = 6 - I_C R_C = 3.45V$$

$$V_E = V_B - U_{BE} = -0.7V$$





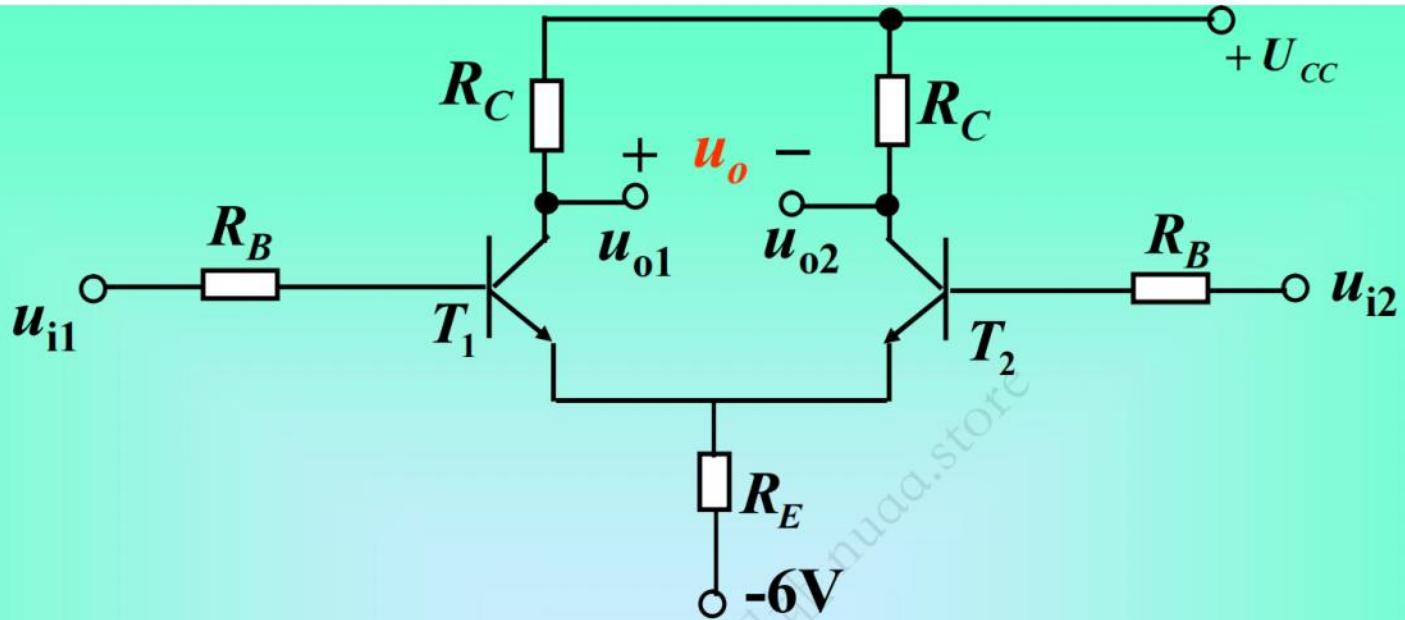
## (2) 信号分解

$$u_{ic1} = u_{ic2} = \frac{u_{i1} + u_{i2}}{2} = 5\text{mV}$$

$$u_{id1} = -u_{id2} = \frac{u_{i1} - u_{i2}}{2} = 2\text{mV}$$

$$u_{i1}=5+2\text{ mV}$$

$$u_{i2}=5-2\text{ mV}$$

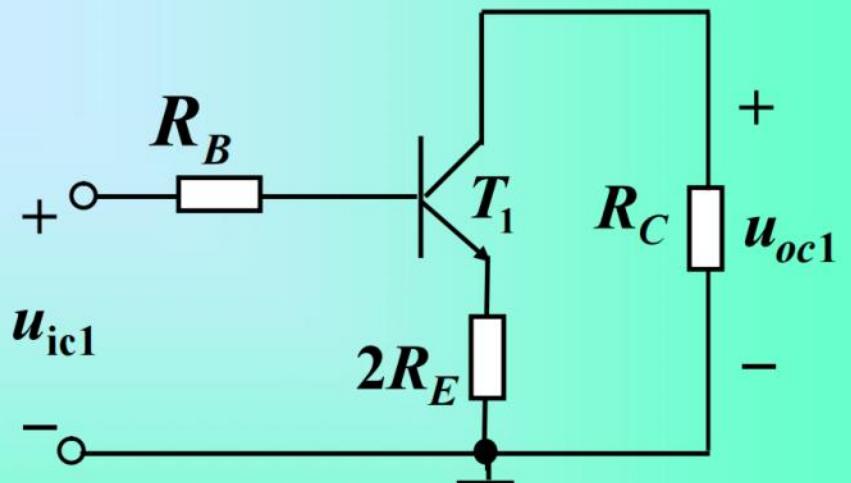


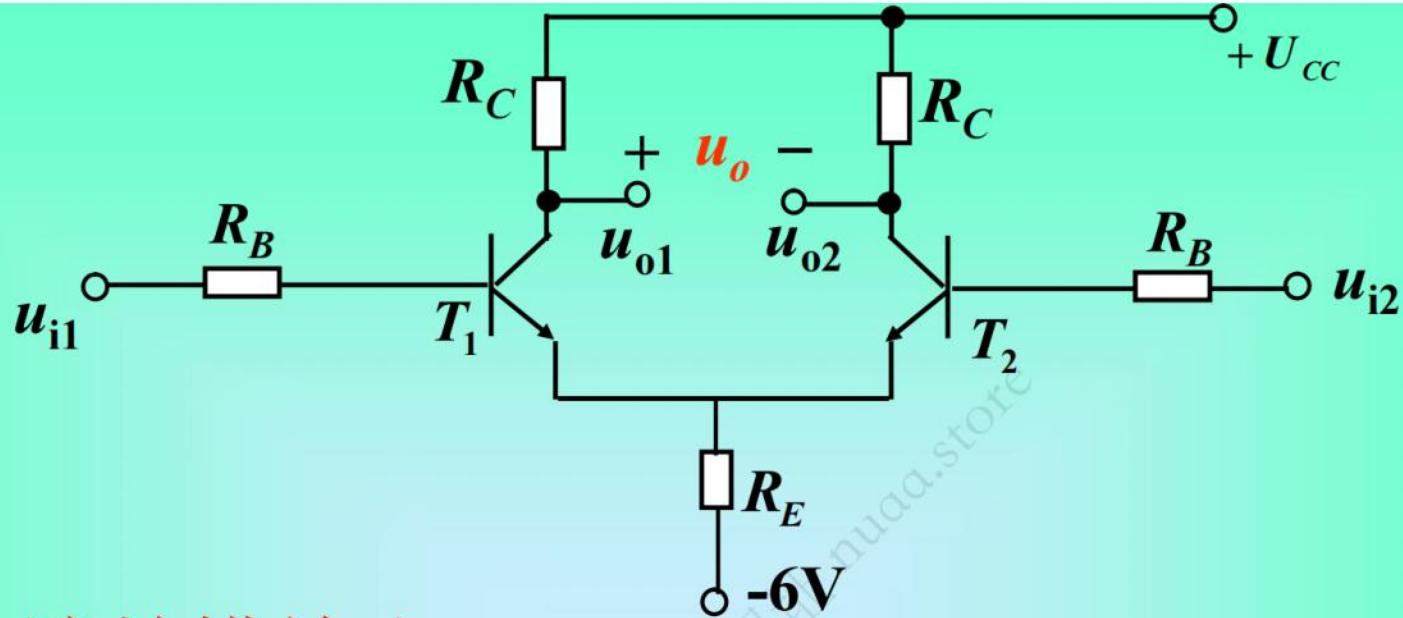
(3) 求单端共模输出

$$A_c = -\beta \frac{R_C}{R_B + r_{be} + 2(1 + \beta)R_E}$$

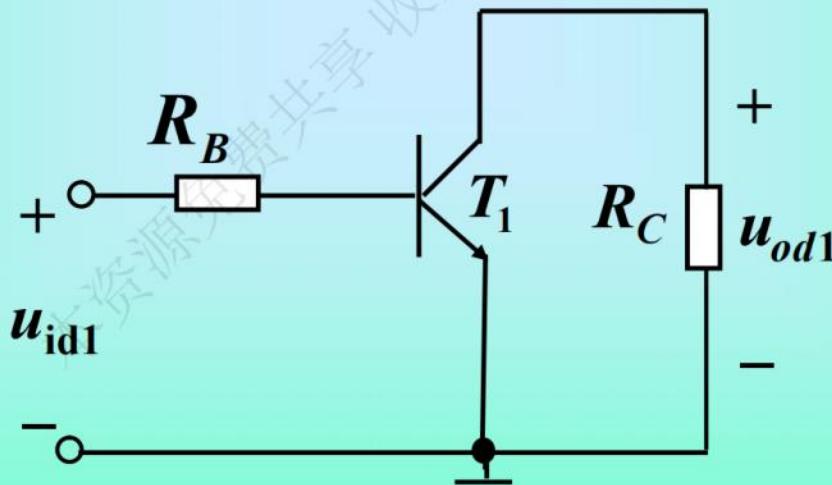
$$u_{oc1} = A_c u_{ic1} \approx -2.5mV$$

$$u_{oc2} = u_{oc1} = -2.5mV$$

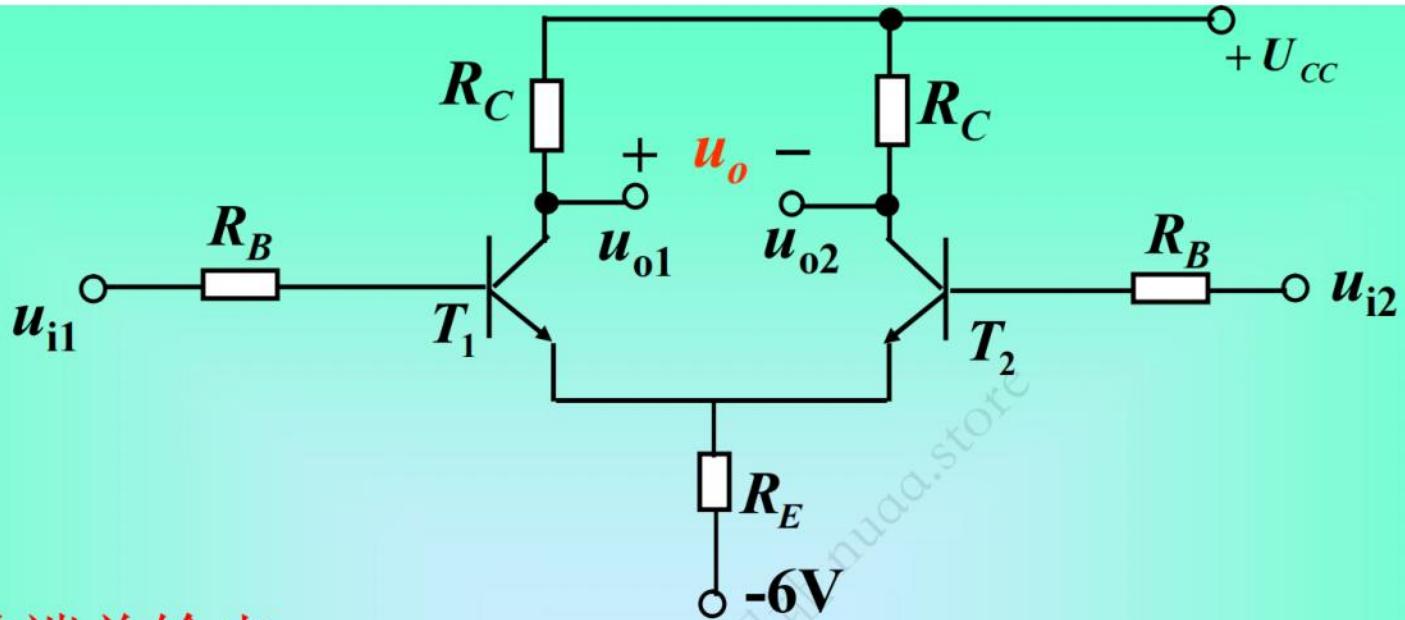




(4) 求单端差模输出



$$u_{od1} = A_{d1} u_{id1} = -\beta \frac{R_C}{R_B + r_{be}} u_{id1} = -40mV \quad u_{od2} = -u_{od1} = 40mV$$



(5) 求单端总输出

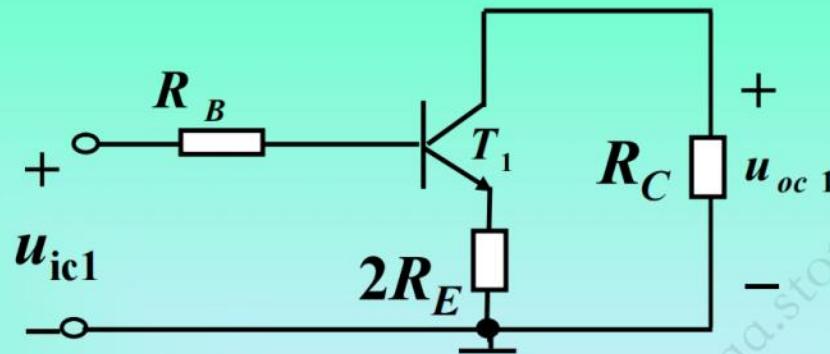
$$u_{o1} = u_{oc1} + u_{od1} = -2.5 - 40 = -42.5 \text{mV}$$

$$u_{o2} = u_{oc2} + u_{od2} = -2.5 + 40 = -37.5 \text{mV}$$

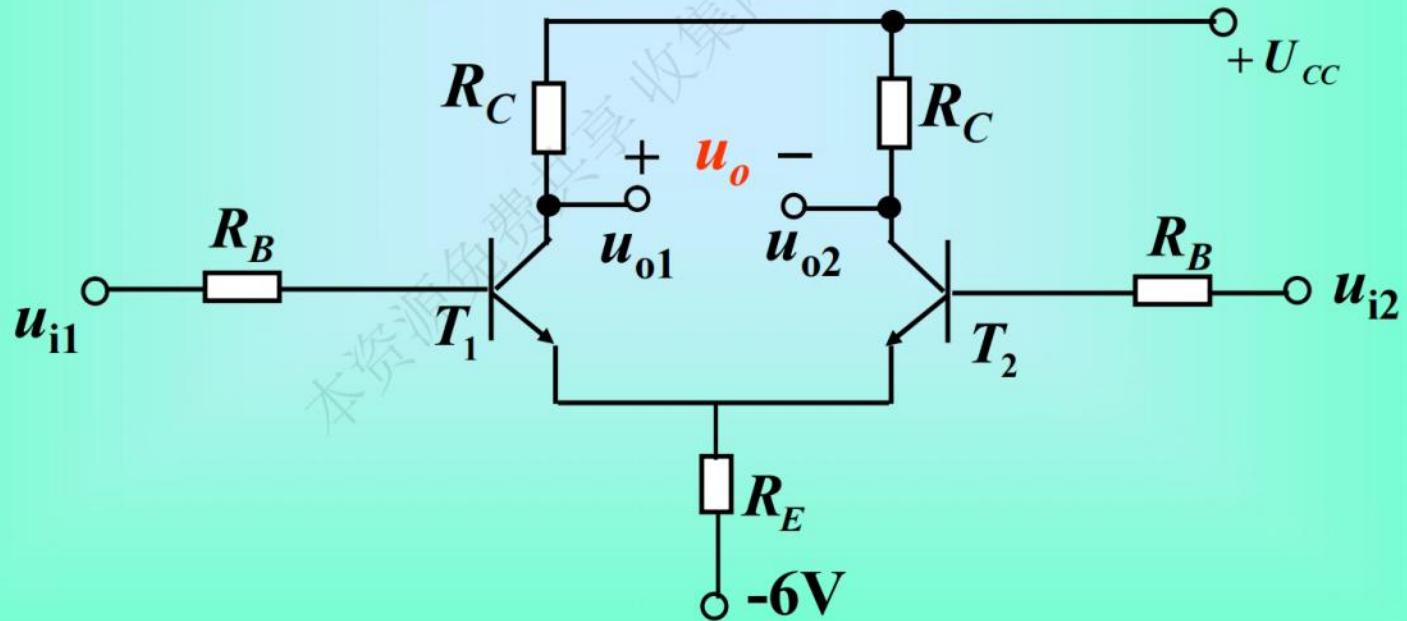
(6) 求双端总输出

$$u_o = u_{o1} - u_{o2} = -80 \text{mV}$$

## (7) 求共模输入电阻及差模输入电阻



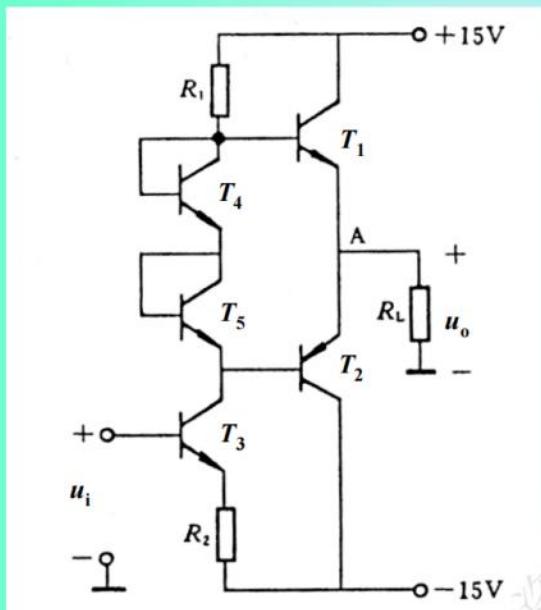
$$r_{ic} = R_B + r_{be} + 2(1 + \beta)R_E$$



$$r_{id} = 2(R_B + r_{be})$$

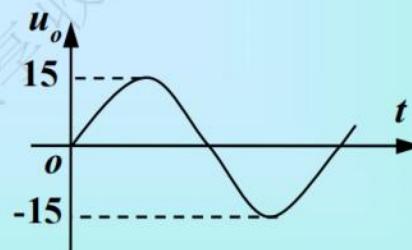
## 2.9

- (1) 图示是什么电路?  $T_4$ 和 $T_5$ 是如何联接的, 起什么作用?
- (2) 在静态时,  $V_A=0$ , 这时 $T_3$ 的集电极电位 $V_{C3}$ 应调到多少? 设各管的发射结电压为0.6V。
- (3) 忽略 $U_{CES}$ , 求最大输出功率 $P_o$



1、 $T_4$ 和 $T_5$ 接成二极管, 消除交越失真

2、 $V_{C3} = -0.6V$



$$P_{o\max} = \frac{U_{o\max}^2}{R_L} = \frac{\left(\frac{15 - U_{CES}}{\sqrt{2}}\right)^2}{R_L} \approx \frac{225/2}{9} = 12.5$$

2.10 在图示的场效应管放大电路中，已知  $R_{G1}=2M\Omega$ ,  $R_{G2}=47k\Omega$ ,  $R_G=10M\Omega$ ,  $R_D=30k\Omega$ ,  $R_S=2k\Omega$ ,  $U_{DD}=18V$ ,  $C_1=C_2=0.01\mu F$ ,  $C_S=10\mu F$ , 管子为3DO1。

试计算：（1）静态值  $I_D$  和  $U_{DS}$ ; （2） $r_i$ ,  $r_o$  和  $A_u$ ;

（3）如将旁路电容  $C_S$  除去，计算  $A_{uf}$ 。

设静态值  $U_{GS}=-0.2V$ ,  $gm=1.2mA/V$ ,  $rds>>RD$ 。

$$V_G = \frac{R_{G2}}{R_{G1} + R_{G2}} U_{DD} = 0.4V$$

$$U_{GS} = V_G - V_S = 0.4 - R_S I_D$$

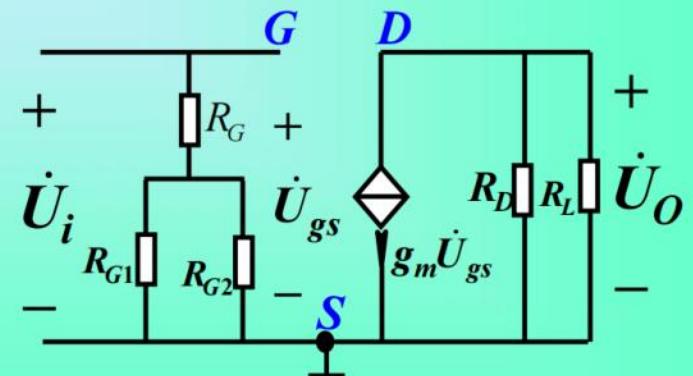
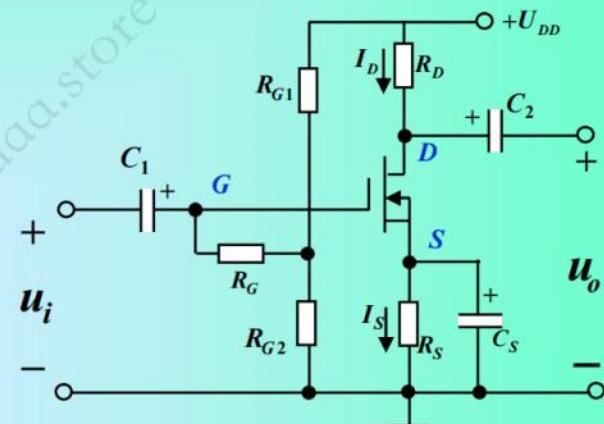
$$\Rightarrow I_D = 0.3mA$$

$$U_{DS} = U_{DD} - (R_D + R_S) I_D = 8.2V$$

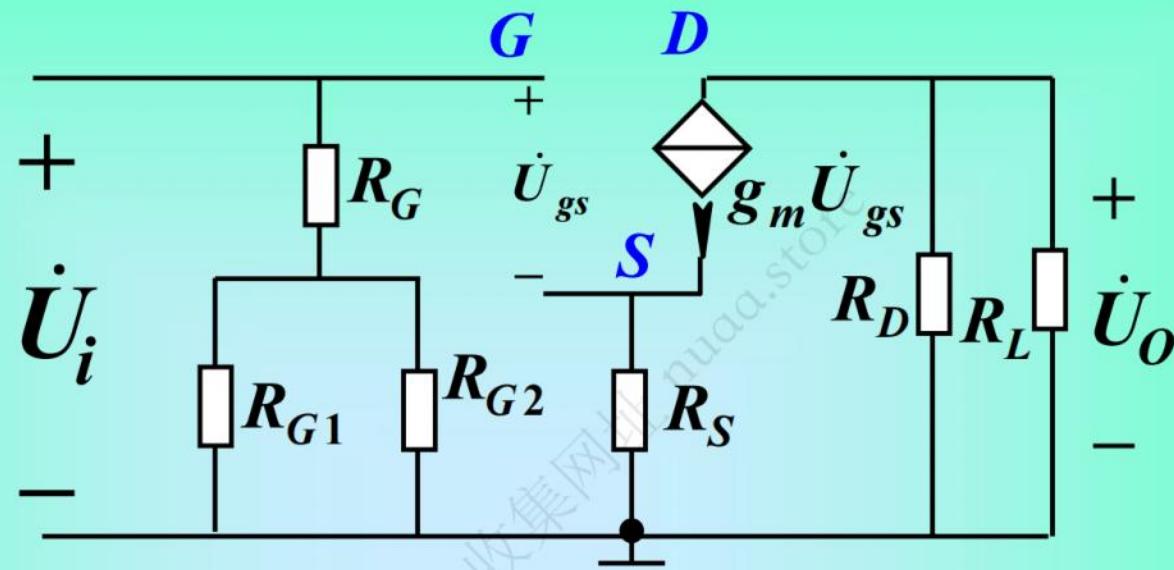
$$A_u = \frac{\dot{U}_o}{\dot{U}_i} = - \frac{g_m \dot{U}_{gs} (R_D // R_L)}{\dot{U}_{gs}} = - g_m R'_L = -36$$

$$r_i = \frac{\dot{U}_i}{\dot{I}_i} = R_G + R_{G1} // R_{G2}$$

$$r_o = R_D$$



(3) 如将旁路电容 $C_s$ 除去, 计算 $A_u$ 。



$$\dot{U}_i = \dot{U}_{gs} + g_m \dot{U}_{gs} R_S$$

$$\dot{U}_o = -g_m \dot{U}_{gs} (R_D // R_L)$$

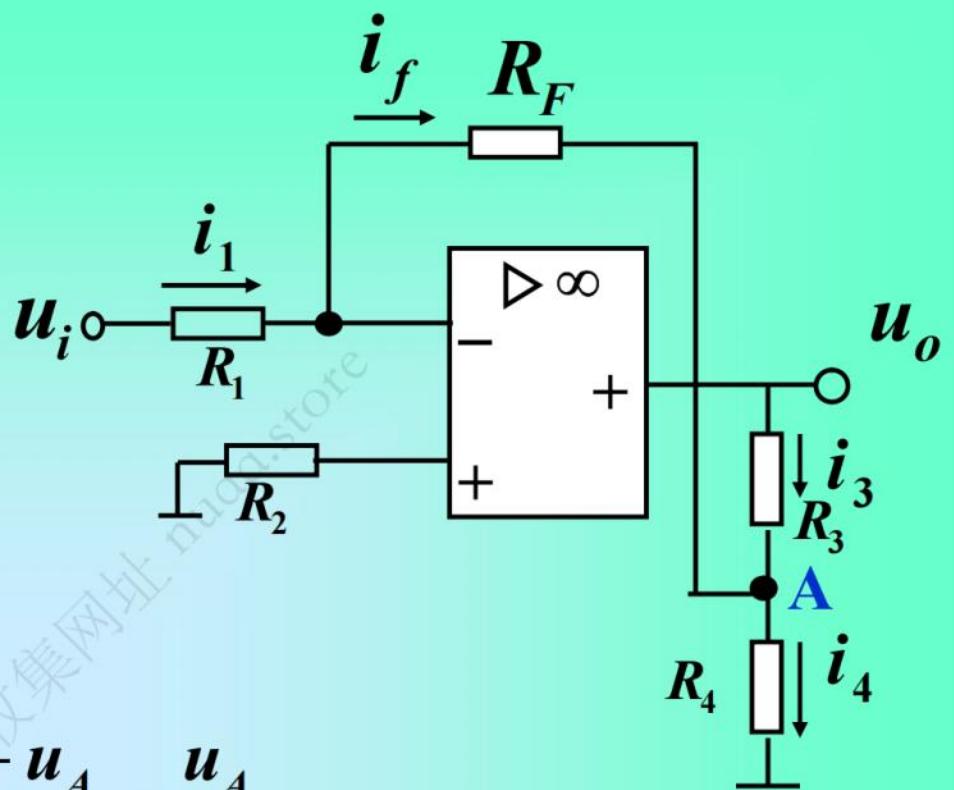
$$A_u = \frac{\dot{U}_o}{\dot{U}_i} = -\frac{g_m R'_L}{1 + g_m R_S} = -10.6$$

3.1

$$i_1 = i_f \rightarrow u_A = -\frac{R_F}{R_1} u_i$$

$$i_f + i_3 = i_4 \rightarrow \frac{u_i}{R_1} + \frac{u_o - u_A}{R_3} = \frac{u_A}{R_4}$$

$$u_o = -5.06u_i$$



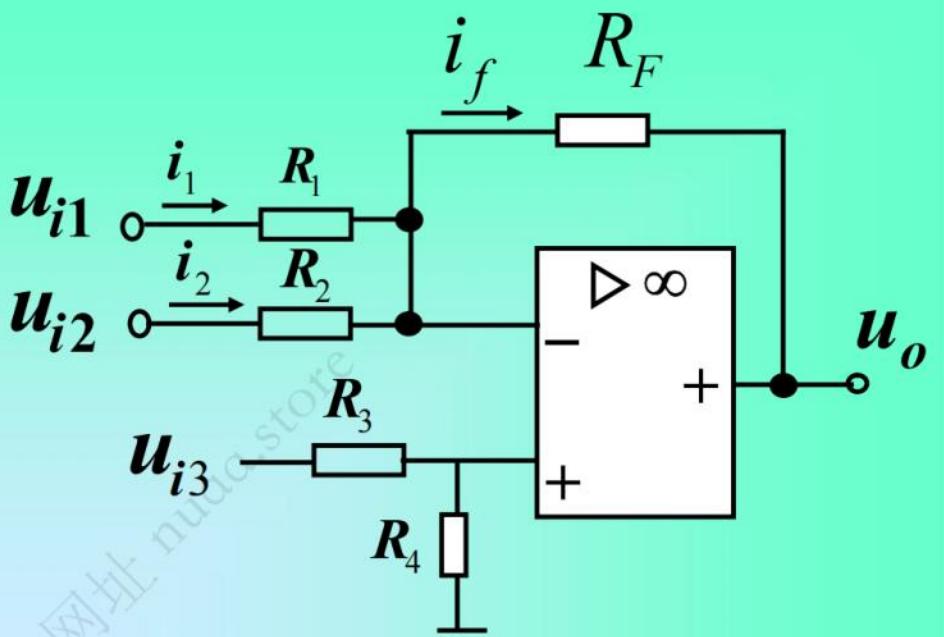
3.2

$$u_- = u_+ = \frac{R_4}{R_4 + R_3} u_{i3}$$

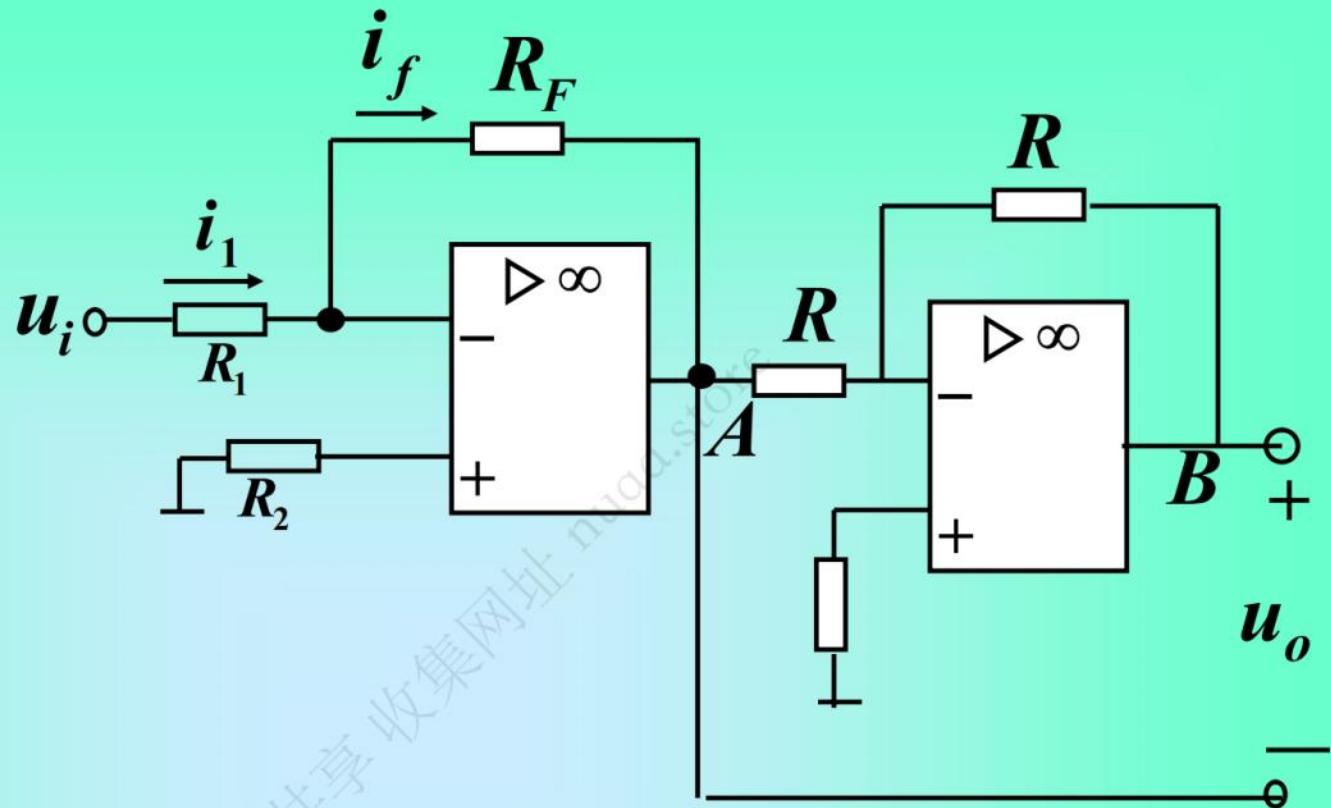
$$i_1 + i_2 = i_f$$

$$\frac{u_{i1} - u_-}{R_1} + \frac{u_{i2} - u_-}{R_2} = \frac{u_- - u_o}{R_f}$$

$$u_o = 0$$



3.3



$$u_A = -\frac{R_F}{R_1} u_i$$

$$u_B = -u_A$$

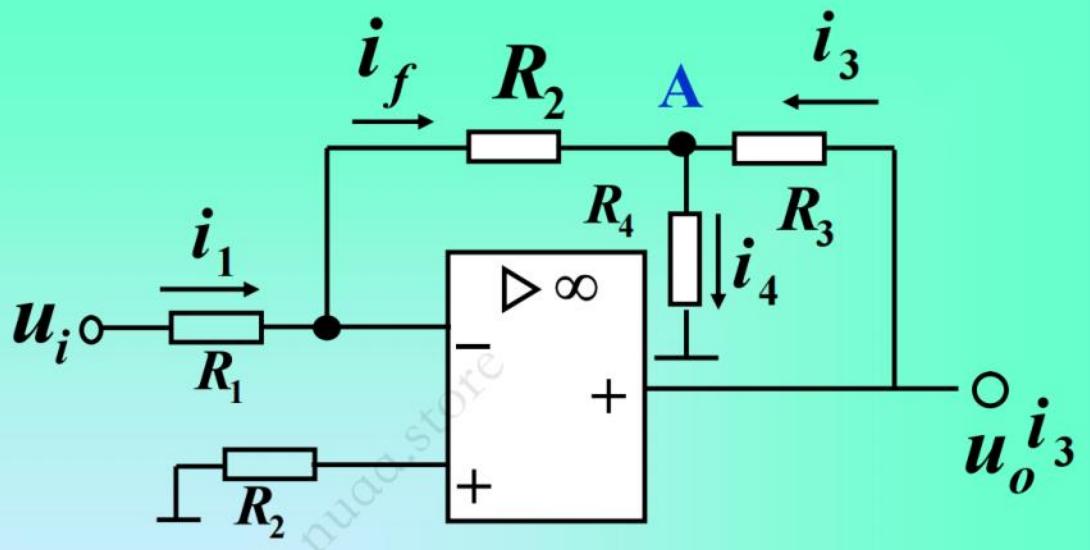
➡  $u_o = u_B - u_A = 2 \frac{R_F}{R_1} u_i$

3.4

$$i_1 = \frac{u_i}{R_1} = i_f$$

$$u_A = -\frac{R_2}{R_1} u_i$$

$$i_f + i_3 = i_4 \quad \Rightarrow \quad \frac{u_i}{R_1} + \frac{u_o - u_A}{R_3} = \frac{u_A}{R_4}$$



### 3.5

$$u_A = u_{i1}$$

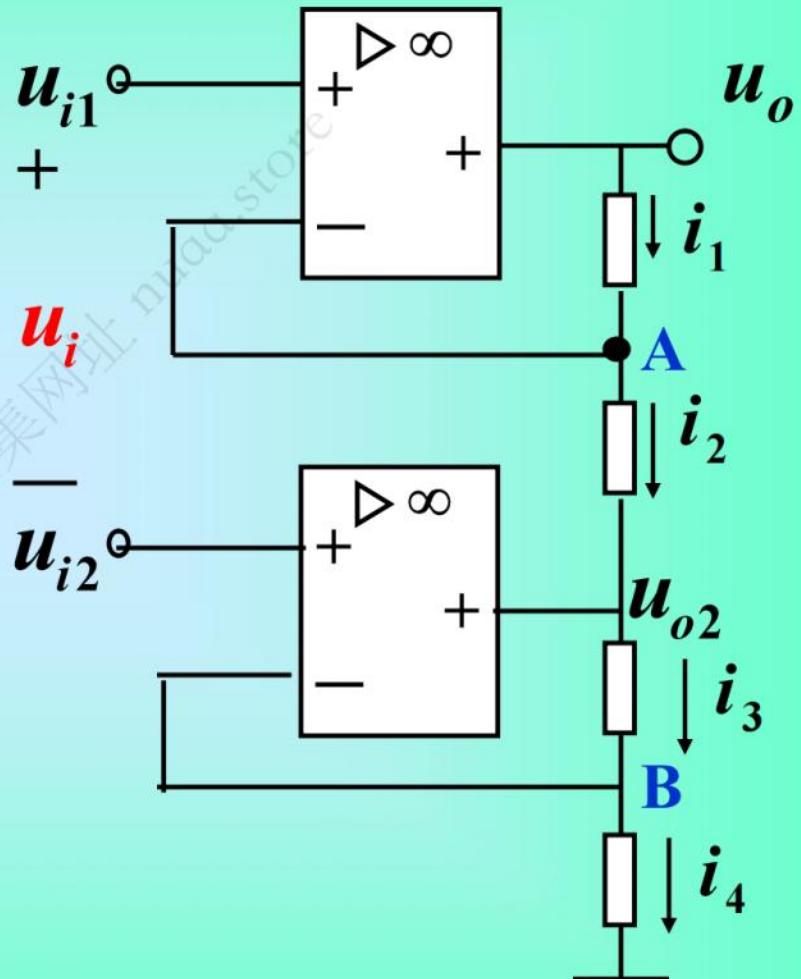
$$u_B = u_{i2}$$

$$u_{o2} = \left(1 + \frac{R}{R}\right)u_{i2} = 2u_{i2}$$

$$i_1 = i_2$$

$$\frac{u_o - u_A}{R} = \frac{u_A - u_{o2}}{R}$$

➡  $u_o = 2u_A - u_{o2} = 2(u_{i1} - u_{i2}) = 2u_i$



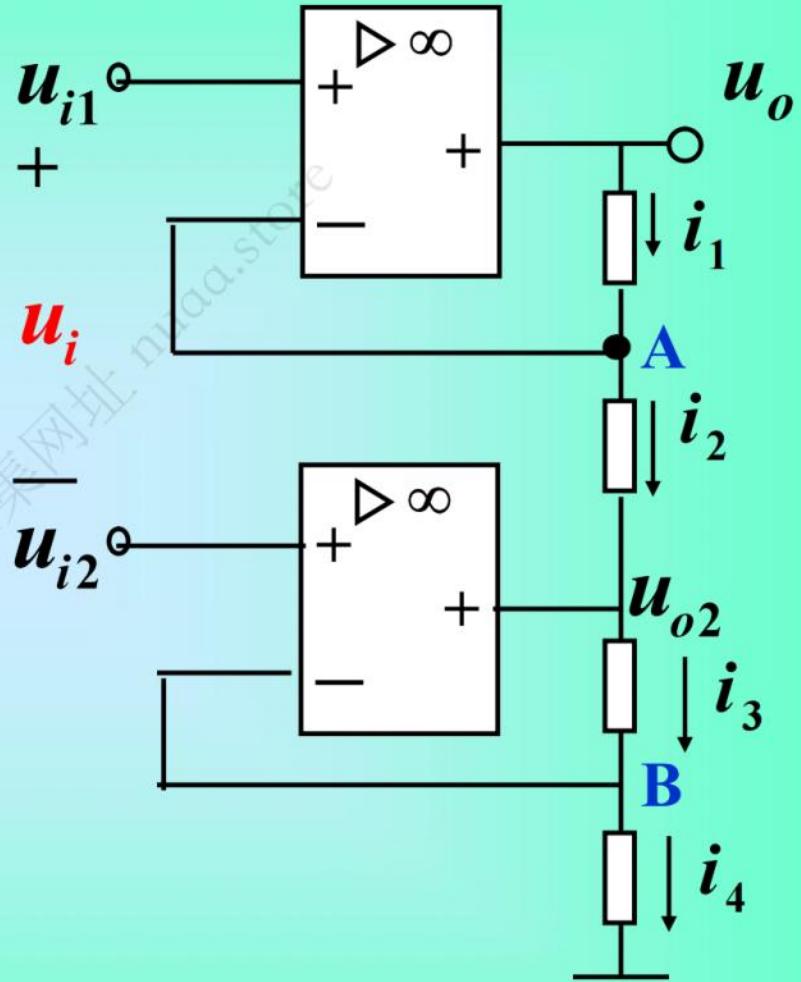
$$i_1 = i_2$$

$$i_3 = i_4$$

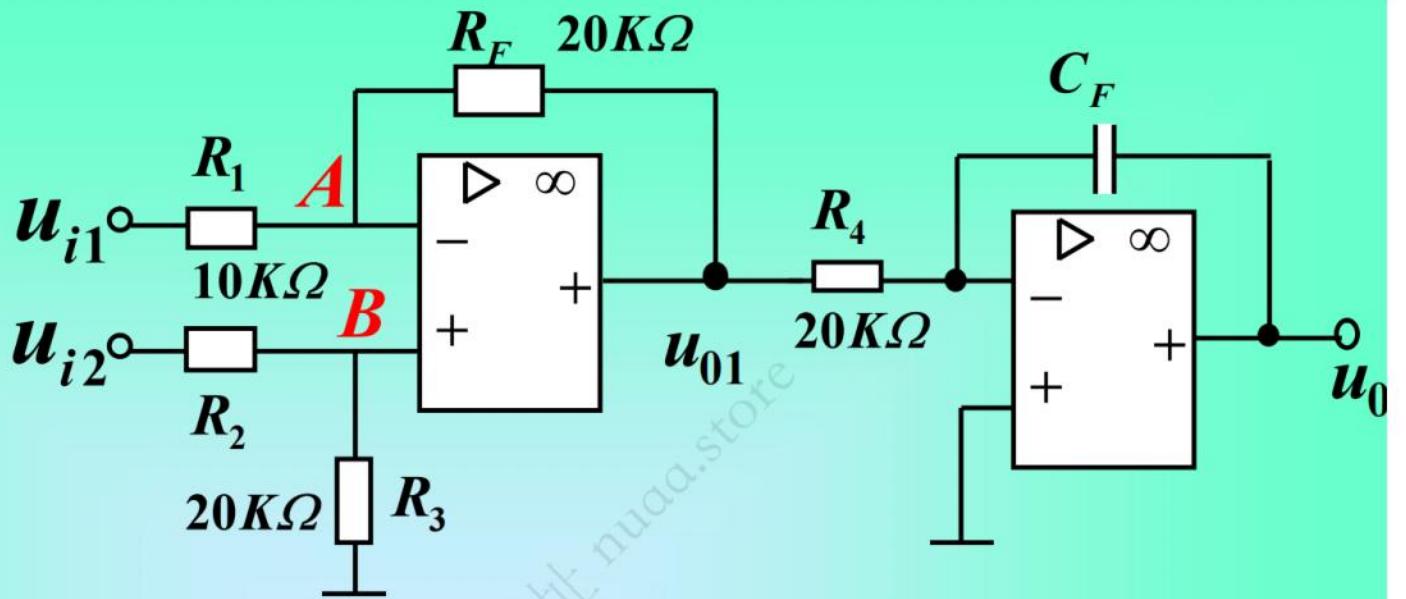
~~$$i_1 = i_2 = i_3 = i_4$$~~

$$\frac{u_o}{4R} = \frac{u_A - u_B}{2R} = \frac{u_{i1} - u_{i2}}{2R}$$

→  $u_o = 2u_i$



3.6

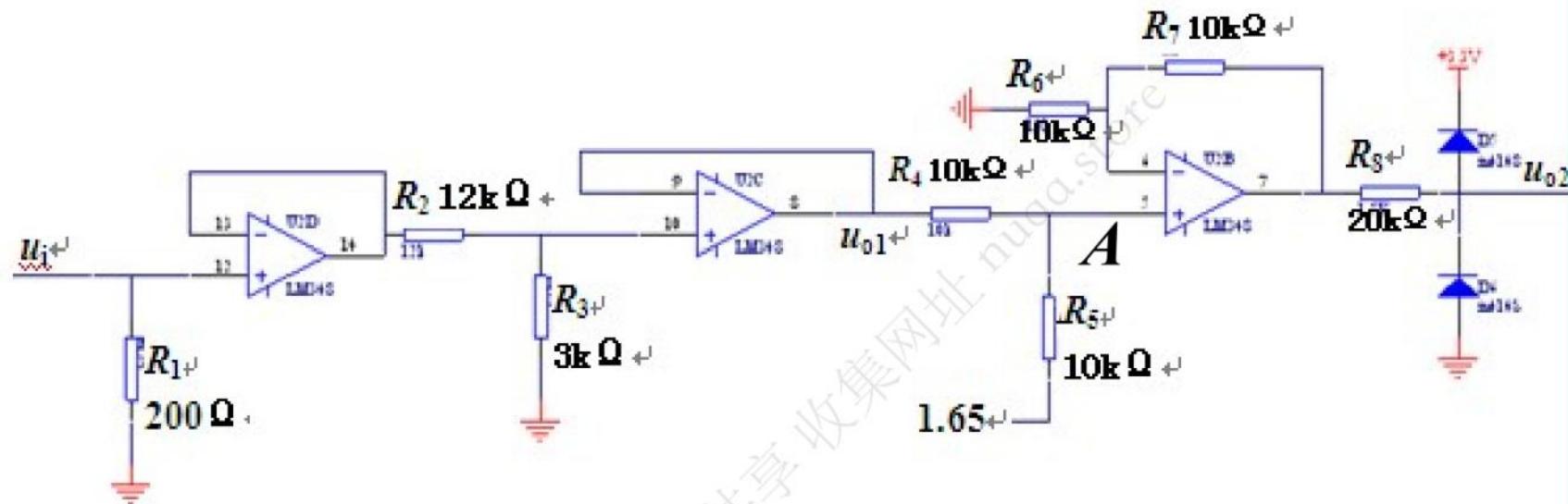


$$u_A = u_B = \frac{R_3}{R_2 + R_3} u_{i2} = \frac{2}{3} V$$

$$\frac{u_{i1} - u_A}{R_1} = \frac{u_A - u_{o1}}{R_F} \rightarrow u_{o1} = -0.2V$$

$$u_o = -\frac{1}{R_4 C_F} \int_0^t u_{o1} dt = 10t \quad t = 1s$$

3.7 下图是一个实际应用的信号调理电路，其最终的输出接入到 CPU 芯片的数据端口，该端口对信号幅值的要求是 0~3.3V,  $u_i$  是一个正弦交流信号，请写出  $u_{o1}$ 、 $u_{o2}$  的表达式，并说明 D1, D2 的作用，以及为何要设计一个 1.65V 的直流输入。



$$u_{o1} = \frac{1}{5} u_i \quad u_A = \frac{u_{o1} + 1.65}{2}$$

$$u_{o2} = \left(1 + \frac{R_7}{R_6}\right) u_A = 2u_A = u_{o1} + 1.65$$

**D1、D2**的作用是为了对端口信号的幅值进行限幅

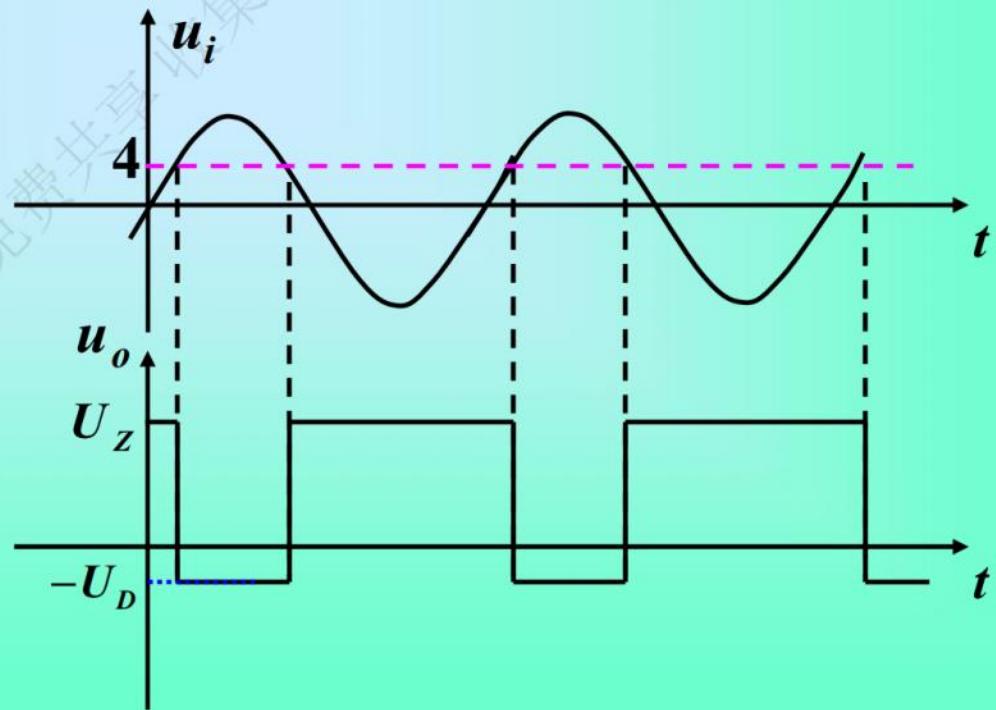
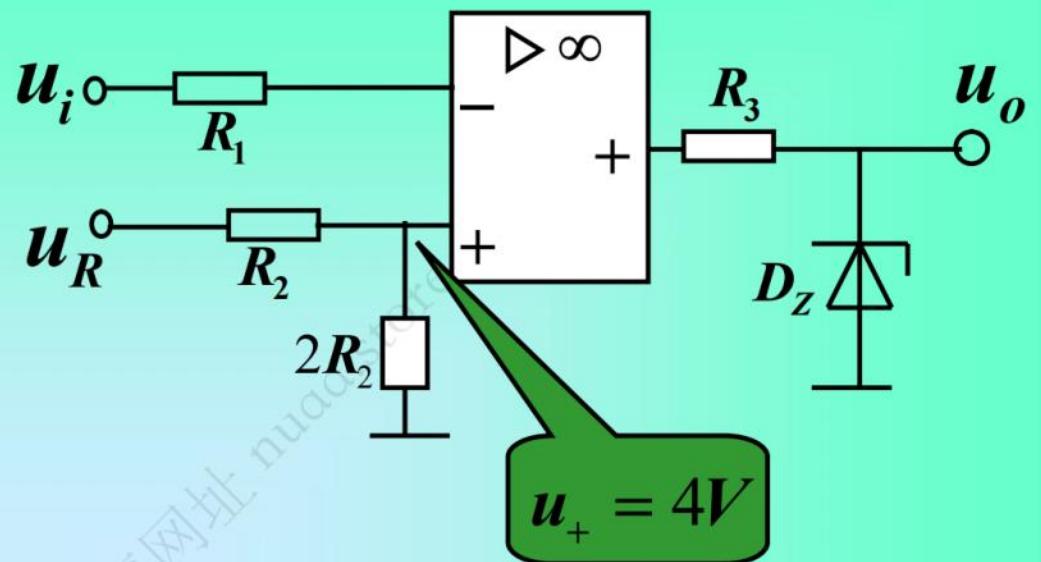
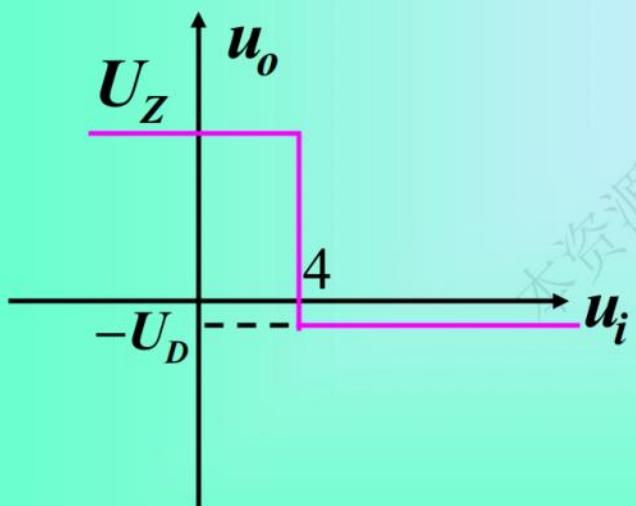
设计一个1.65的直流输入是为了提高交流信号的输入范围

3.8

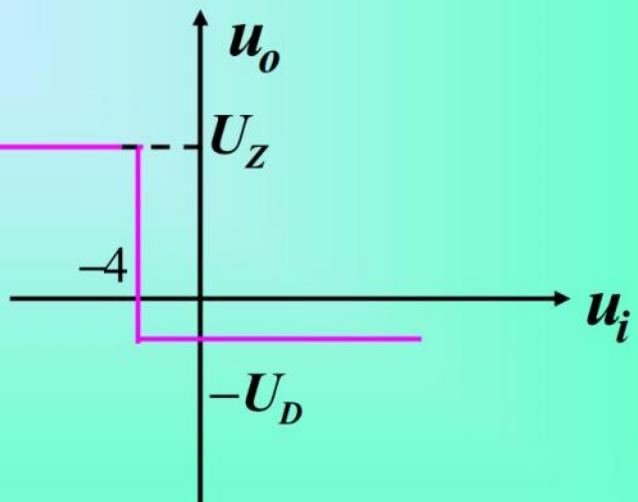
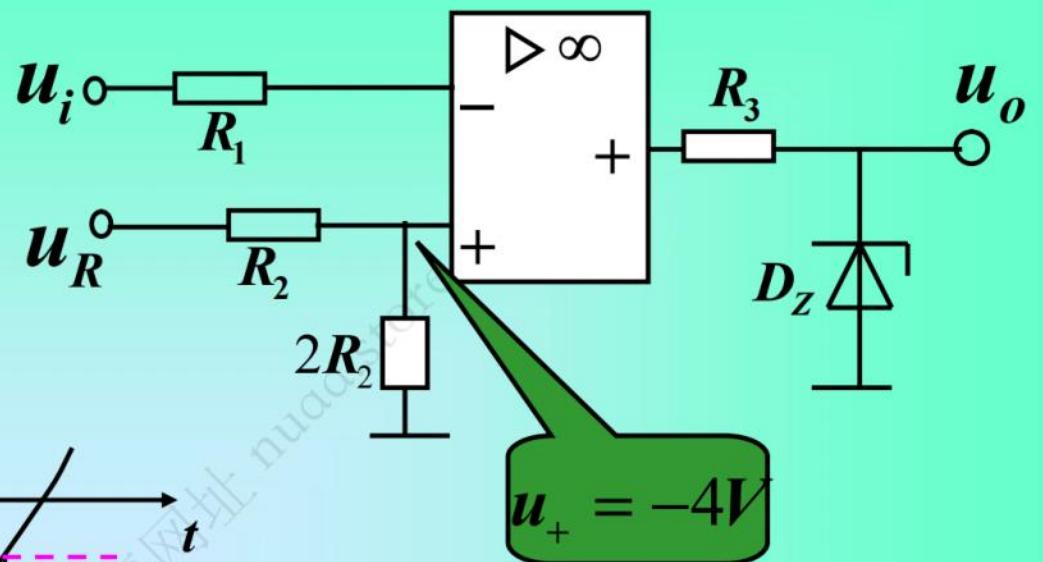
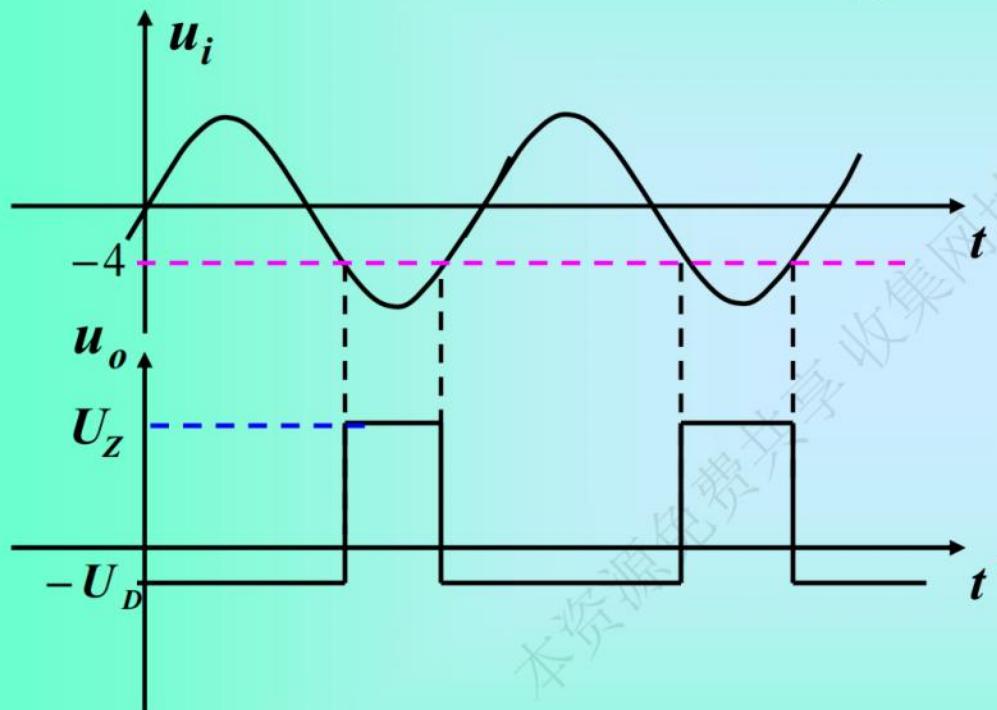
$$u_i > u_+ \Rightarrow u_o = -U_D = -0.7V$$

$$u_i < u_+ \Rightarrow u_o = U_Z = 6V$$

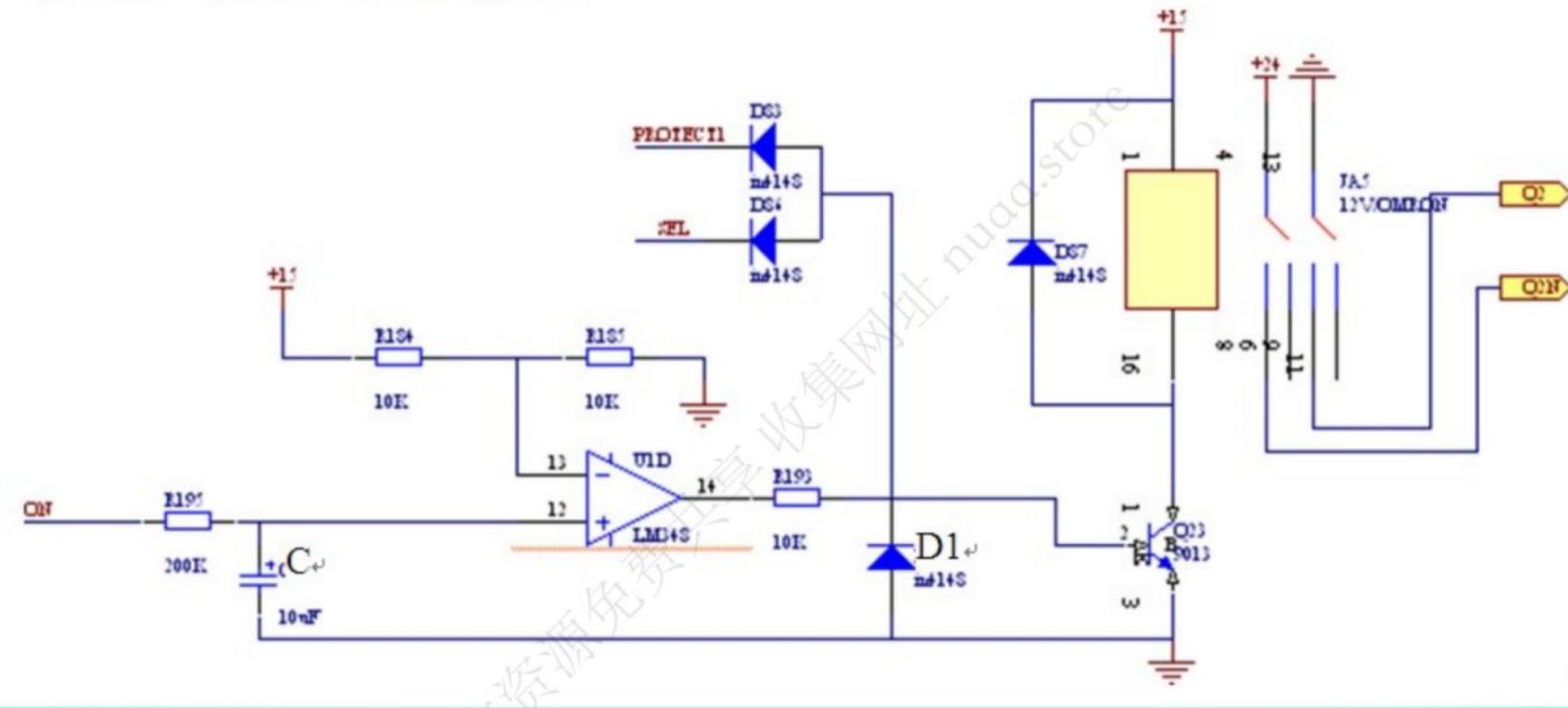
$$1. \quad u_R = 6V$$



$$2、 u_R = -6V$$

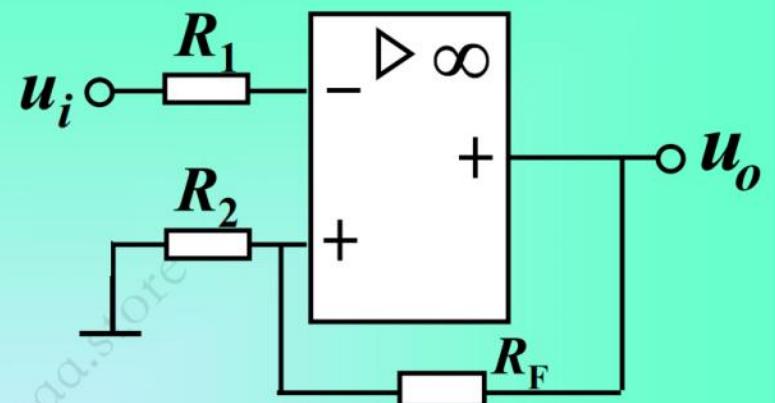
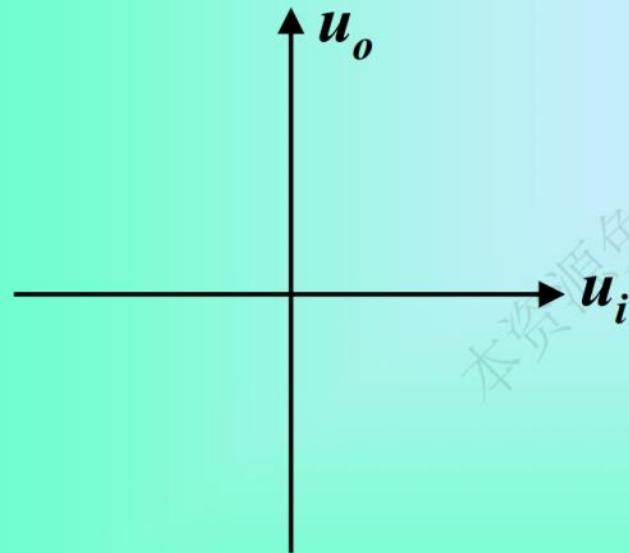
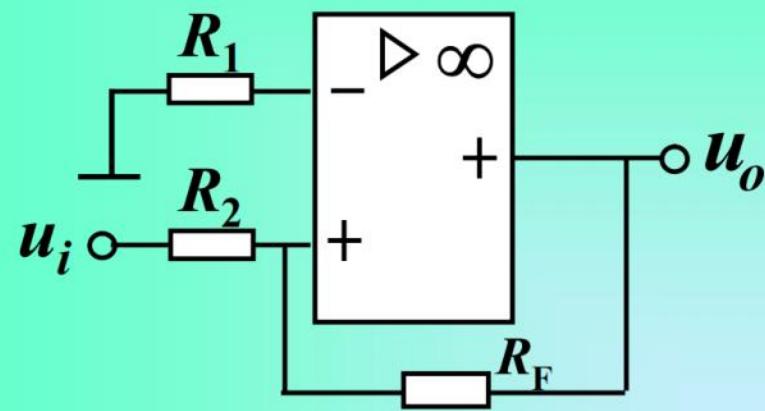


3.10 下图是一个实用的控制电路，ON, PROTECT1, SEL 均为输入信号，其幅值或者是 0V，或者是 15V，请分析在什么情况下 Q2, Q2N 这两个端子能获得 24V 的电压(该电压用于控制接触器)，并说明 C 和 D1 的作用。

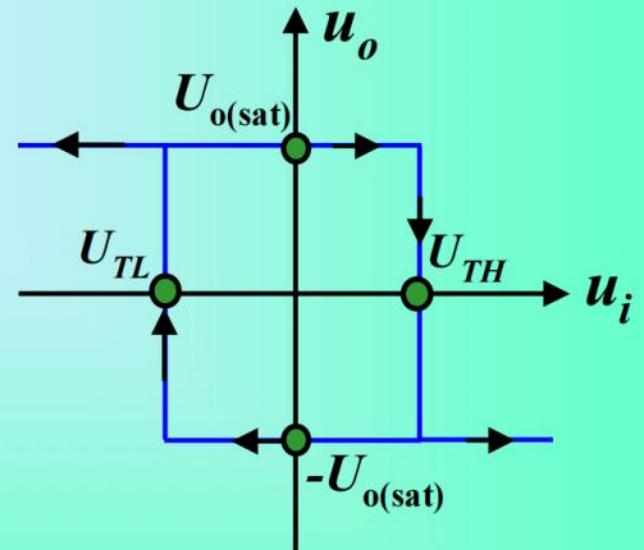


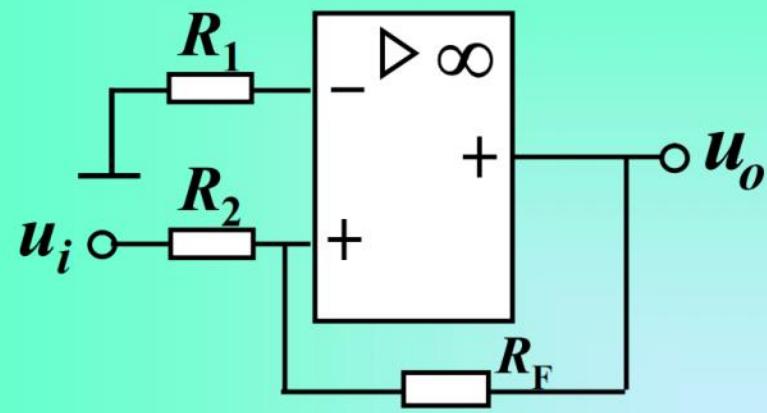
在三个输入信号均为**15V**的时候**Q2、Q2N**能获得**24V**的电压  
**C与200kΩ**的电阻组成延时电路。**D1**防止T发射结被反向击穿。

# 课后作业



滞回比较器

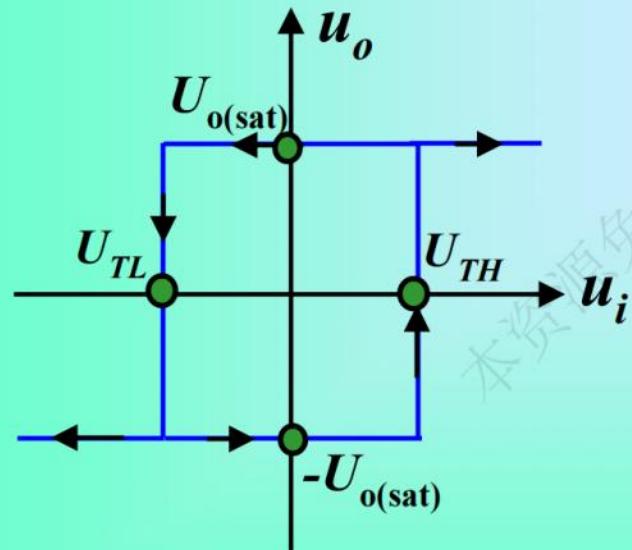




设加电源瞬间,  $u_i < 0$

$$u_o = -U_{o(sat)} \Rightarrow u_+ = -\frac{R_2}{R_2 + R_F} U_{o(sat)} + \frac{R_F}{R_2 + R_F} u_i$$

$u_i \uparrow \Rightarrow$  只有  $u_+ > 0$ ,  $u_o = U_{o(sat)}$

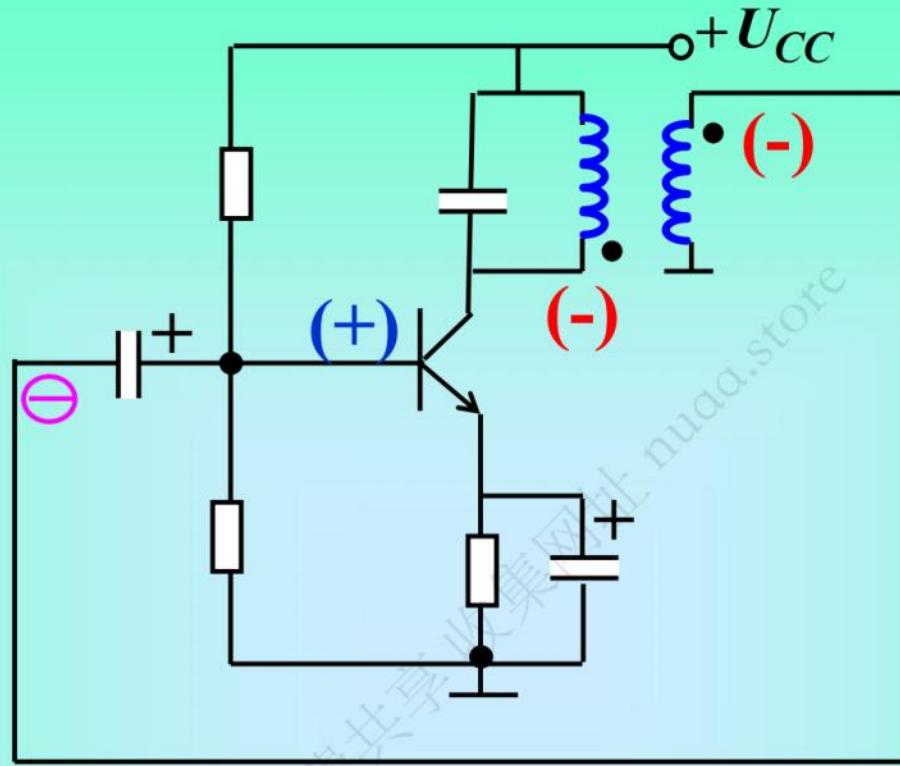


$u_i$  继续  $\uparrow \Rightarrow u_o = U_{o(sat)}$

若  $u_i \downarrow$

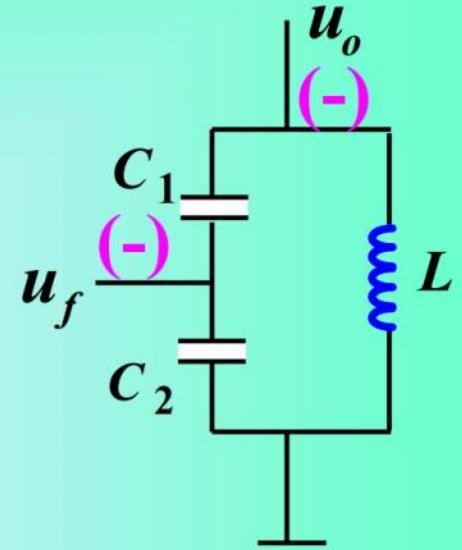
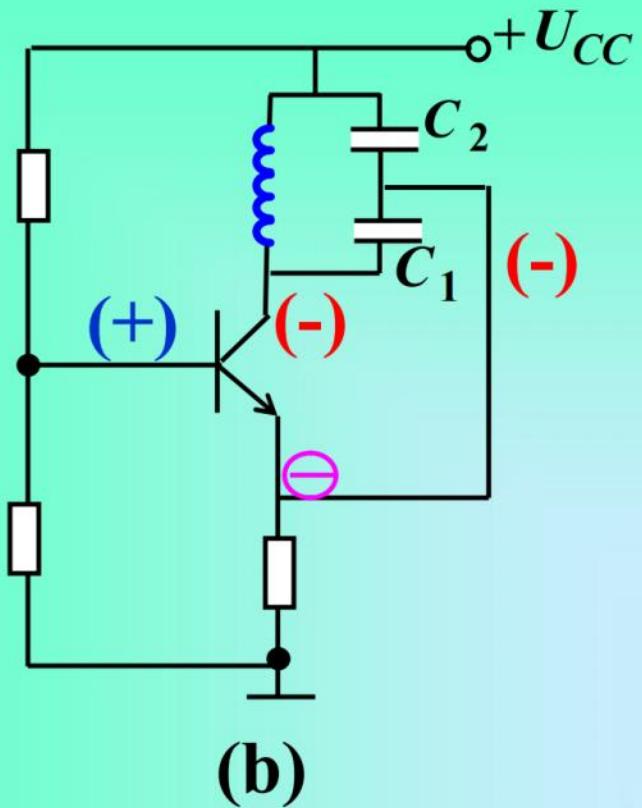
$$\Rightarrow u_i = -\frac{R_2}{R_F} U_{o(sat)} \Rightarrow u_o = -U_{o(sat)}$$

4.1



(a)

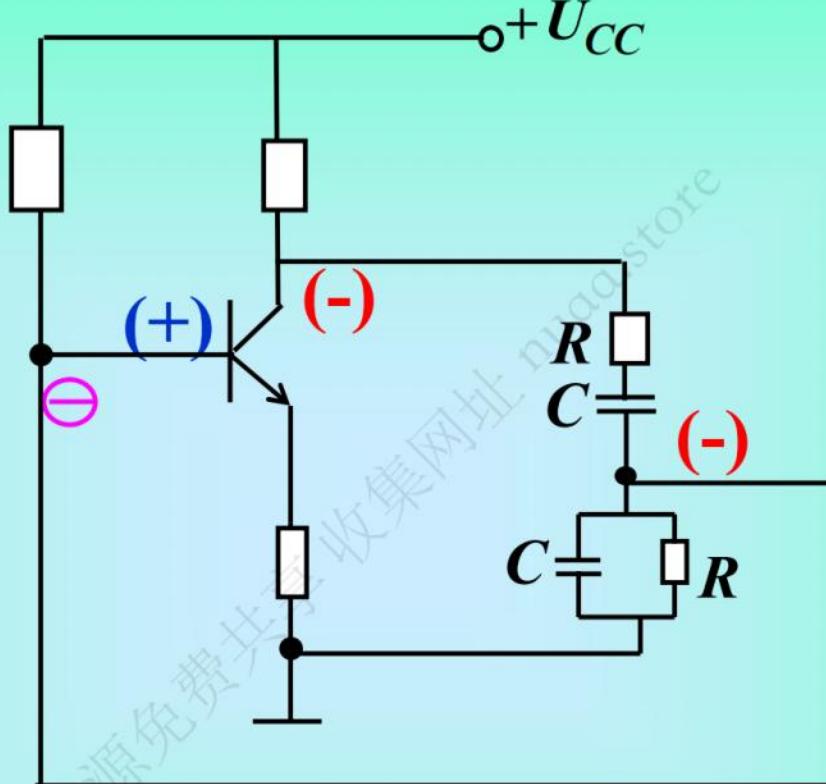
负反馈，无法振荡



$$\frac{\dot{U}_f}{\dot{U}_o} = \frac{\frac{1}{j\omega C_2}}{\frac{1}{j\omega C_1} + \frac{1}{j\omega C_2}} = \frac{\frac{1}{C_2}}{\frac{1}{C_1} + \frac{1}{C_2}} > 0$$

正反馈，可以振荡

4.2



(a)

负反馈

5.1 已知负载电阻  $R_L = 20\Omega$ ，采用单相桥式整流滤波电路供电，要求负载电压  $U_o = 12V$ ，请给出二极管及滤波电容器件的选型依据。如果采用二极管半波整流滤波电路呢？

### (1) 桥式整流滤波

$$I_o = \frac{U_o}{R_L} = 0.6A \quad I_D = \frac{1}{2} I_o = 0.3A$$

$$U_o = 1.2U \quad U_{DRM} = \sqrt{2}U = \sqrt{2} \frac{U_o}{1.2} = 14V$$

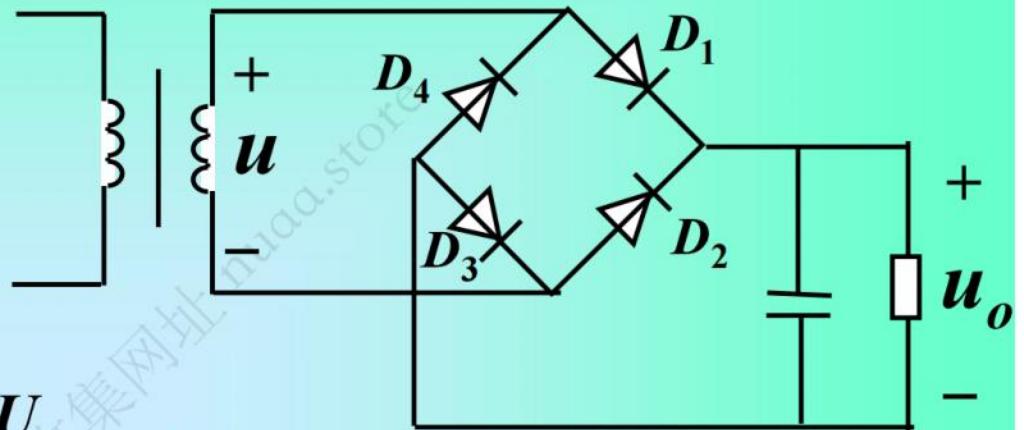
$$U_{CM} = \sqrt{2}U = 14 \quad R_L C = 5T \Rightarrow C = 2500\mu F$$

### (2) 半波整流滤波

$$U_o = U \quad I_o = \frac{U_o}{R_L} = 0.6$$

$$I_D = I_o = 0.6$$

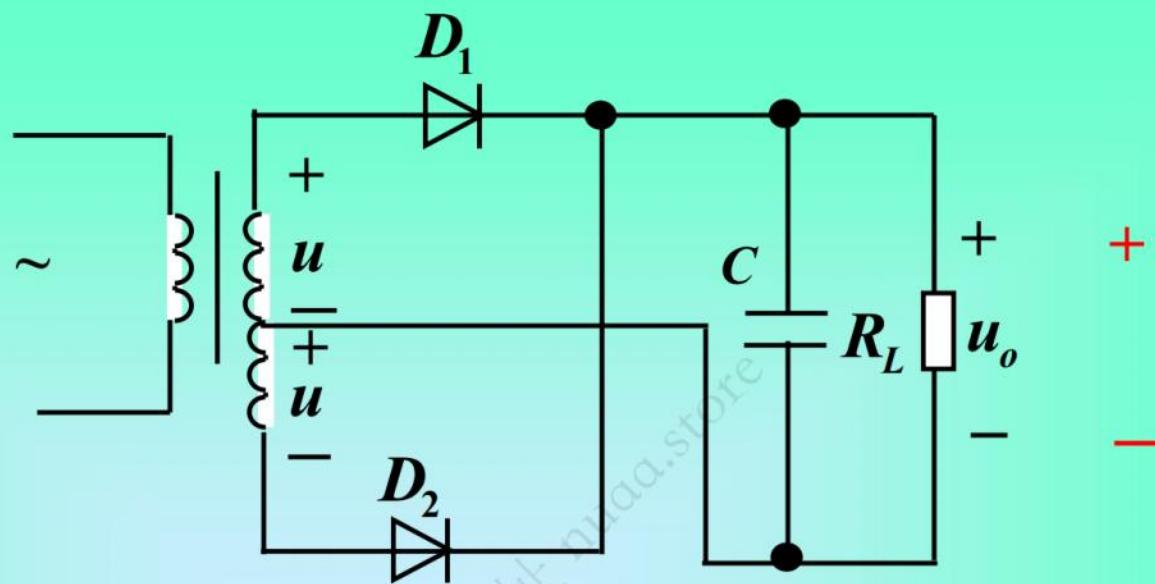
$$U_{DRM} = 2\sqrt{2}U = 2\sqrt{2}U_o = 34$$



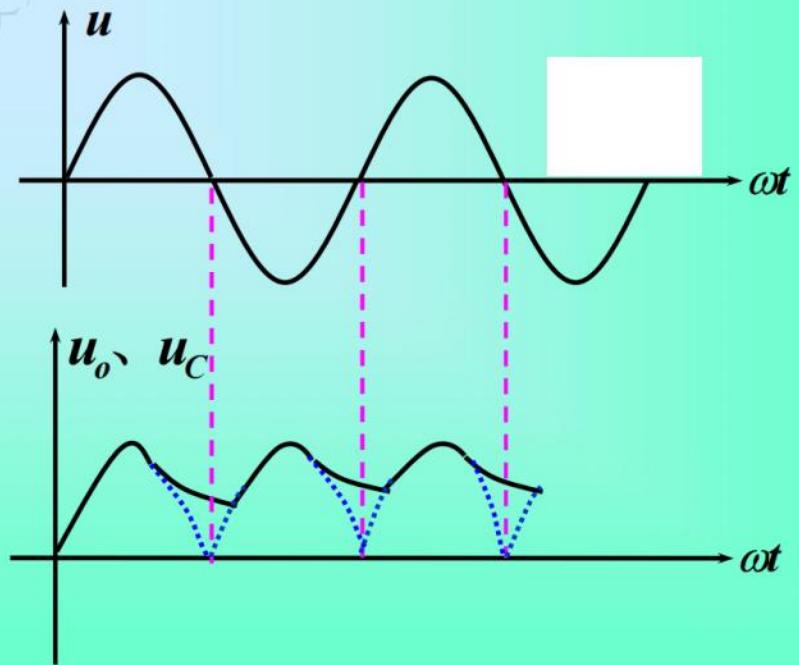
$$U_{CM} = \sqrt{2}U = 17$$

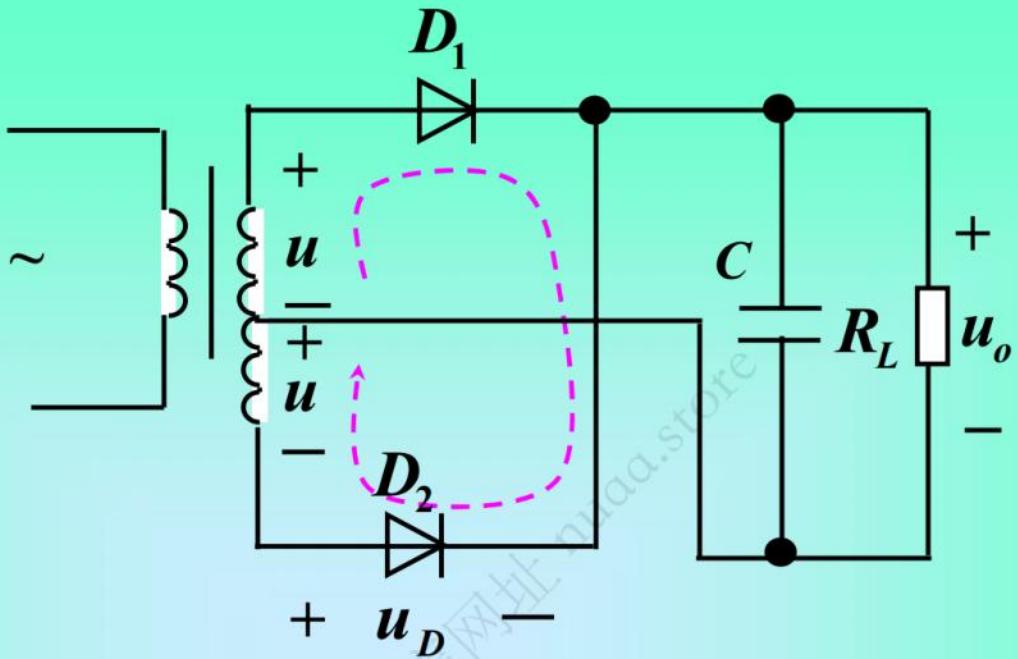
$$R_L C = 5T \Rightarrow C = 2500\mu F$$

5. 2



(2) 全波整流

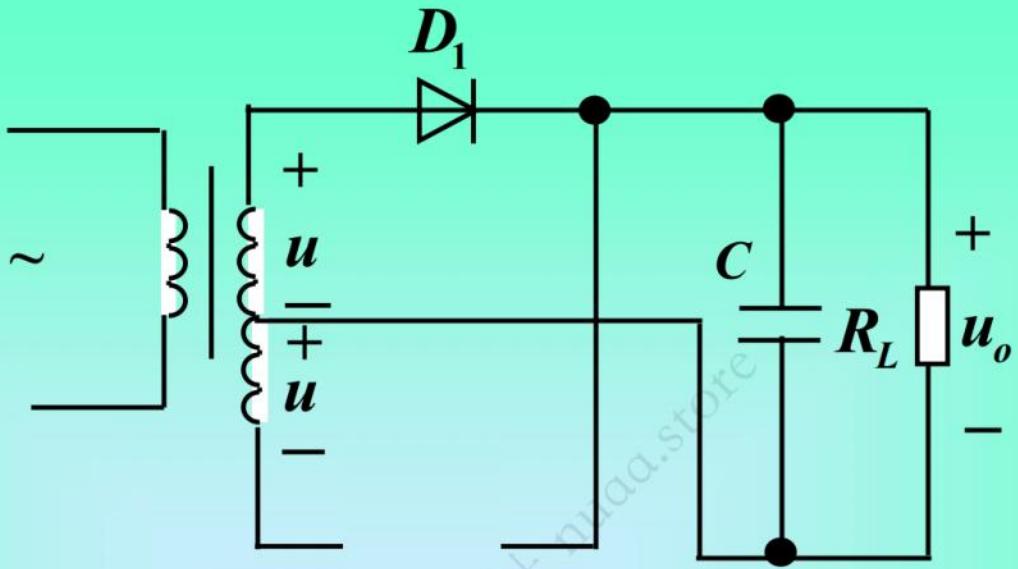




(3) 无  $C$  则  $U_o = 0.9U$ , 有  $C$  则  $U_o = 1.2U$

$$(4) U_{DRM} = 2\sqrt{2}U$$

$$u_D = -2u$$

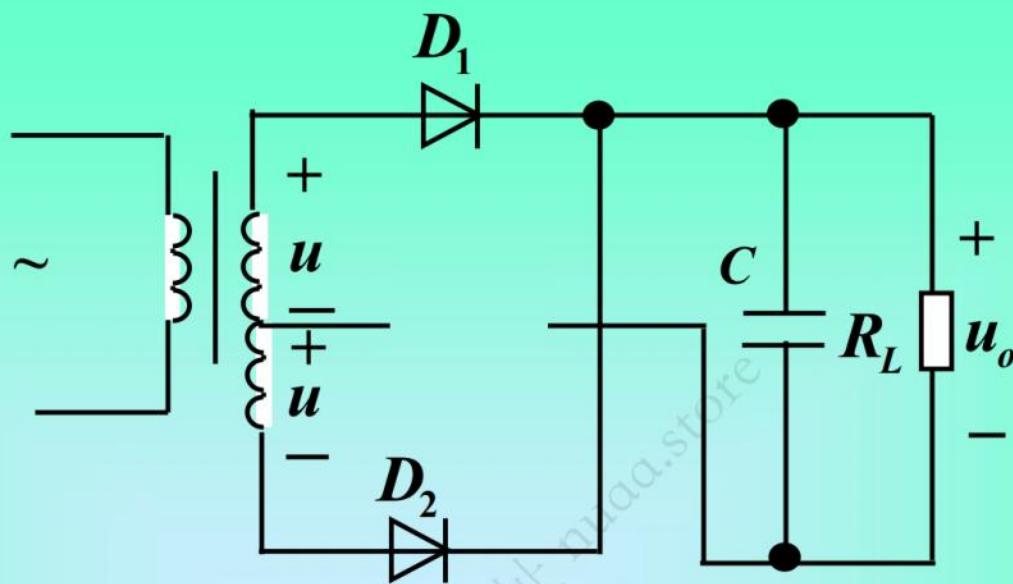


(5)

如果D2虚焊，

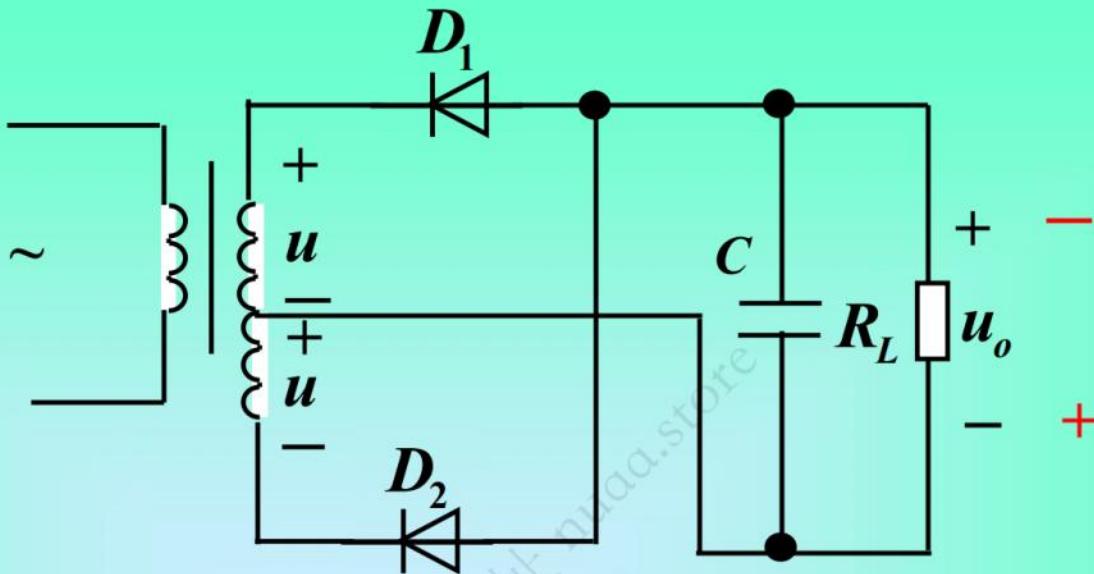
$$U_o = U \neq \frac{1}{2} \cdot 1.2U$$

(5)



如果变压器副边中心抽头虚焊,

输出电压= 0



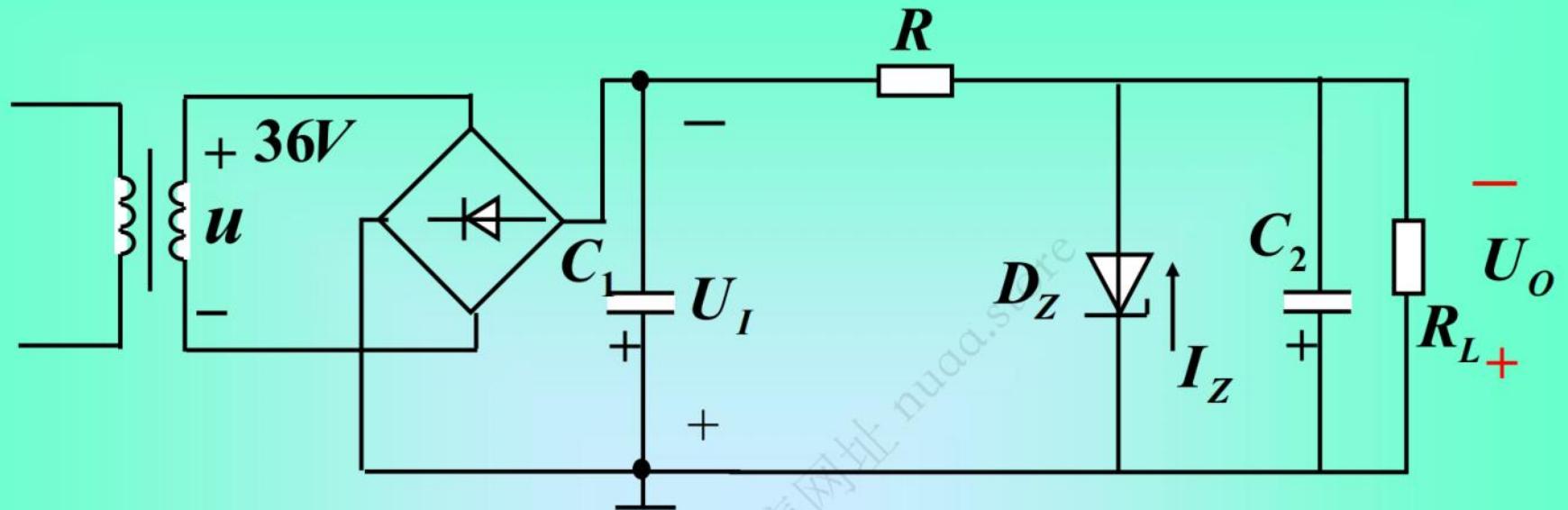
(6) 如果把**D2**的极性接反

变压器副边短路

(7) 如果把图中的**D1**和**D2**都反接

仍有整流滤波作用，输出电压极性相反，滤波电容极性也相反

5. 3



(1)  $U_o = U_z = 15V$

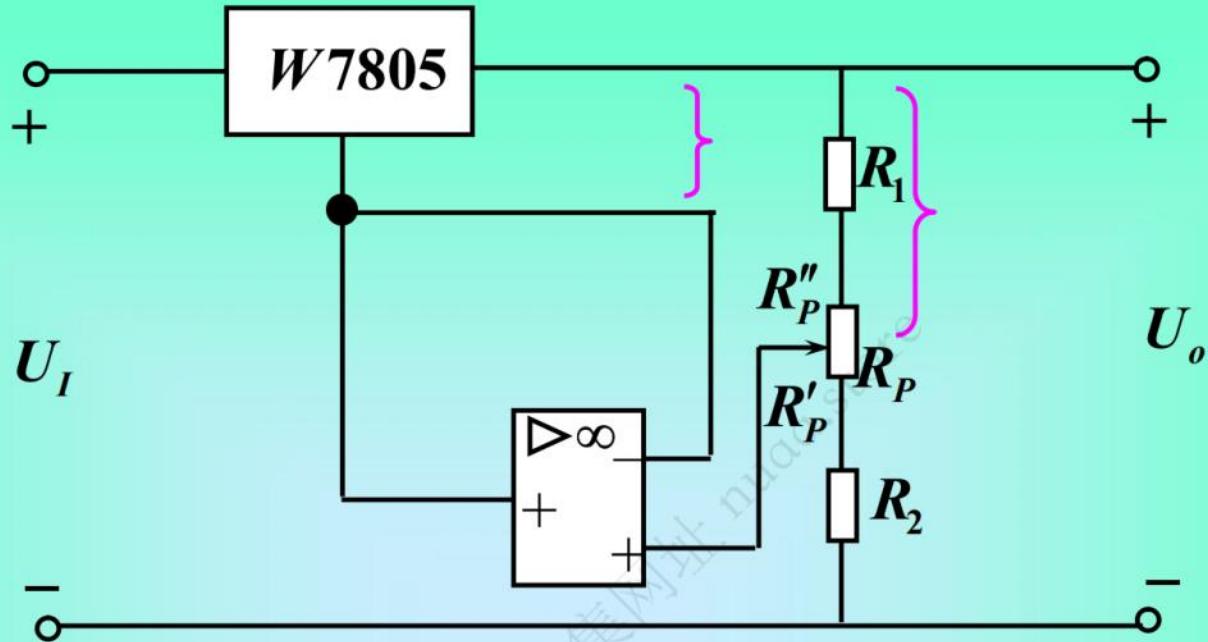
(2)  $U_{C1(\max)} = \sqrt{2}U = 50.9V, U_{C2} = U_z = 15V$

(3)  $I_{z\min} \leq \frac{U_I - U_z}{R} - \frac{U_z}{R_L} \leq I_{z\max} \Rightarrow 5 \leq \frac{43.2 - 15}{2.4} - \frac{15}{R_L} \leq I_{z\max} \Rightarrow 2.22k\Omega < R_L$

(4)  $D_Z$ 接反 则 $D_Z$ 正向导通,  $U_O = 0.7V$

(5)  $R=0$  稳压效果差,  $D_Z$ 可能被烧毁

5. 4

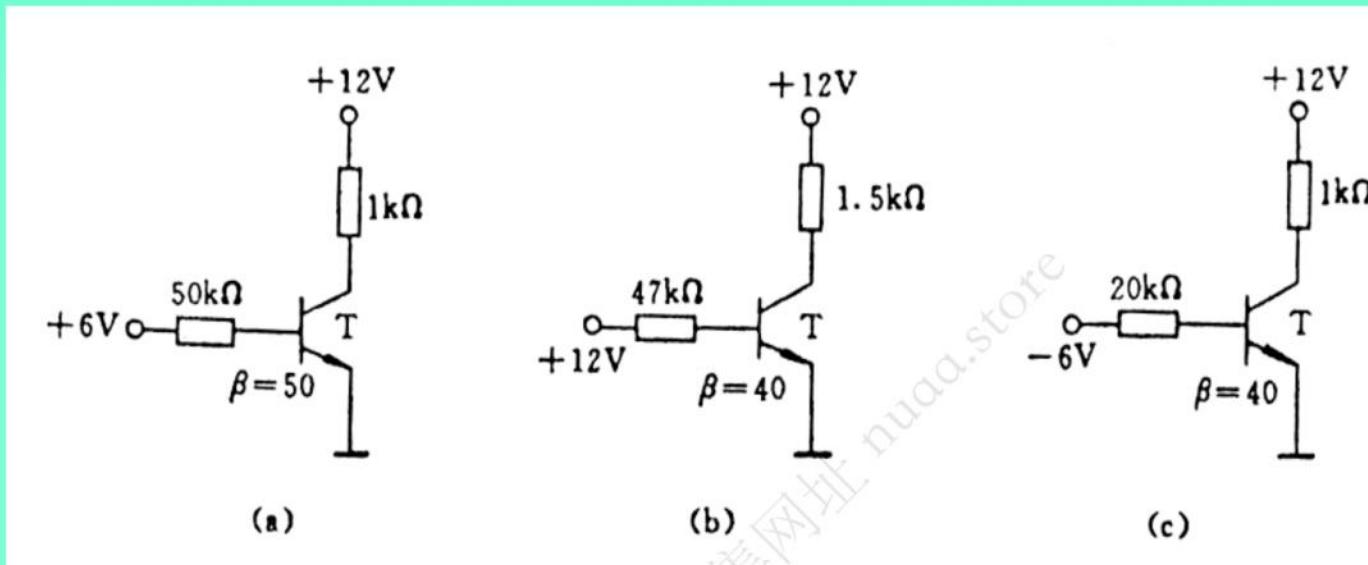


$$\frac{R_1 + R_P''}{R_1 + R_2 + R_P} U_o = 5$$

$$\therefore U_o = \frac{R_1 + R_2 + R_P}{R_1 + R_P''} U_{xx} \quad R_P'' \in [0, R_P]$$

$$\Rightarrow U_o \in [7, 17.3]V$$

6.1在图示的各个电路中，试问晶体管工作于何种状态？



$$I_B = \frac{6 - 0.7}{50} = 0.1\text{mA}$$

$$I_B \geq I_{BS}$$

截止

$$I_{BS} = \frac{12}{1 \cdot 50} = 0.24\text{mA}$$

饱和

$$I_B < I_{BS}$$

放大

6.2 在图示的晶体管“非”门电路中，（1）设 $R_K=3\text{ k}\Omega$ ,  $R_B=30\text{ k}\Omega$ ,

试问晶体管的 $\beta$ 值最小应该是多少才能满足饱和的条件？

（2）设 $\beta=30$ ,  $R_B=30\text{ k}\Omega$ , 试问 $R_K$ 的阻值最大应该是多少才能满足饱和的条件？

$$I_B \geq I_{BS}$$

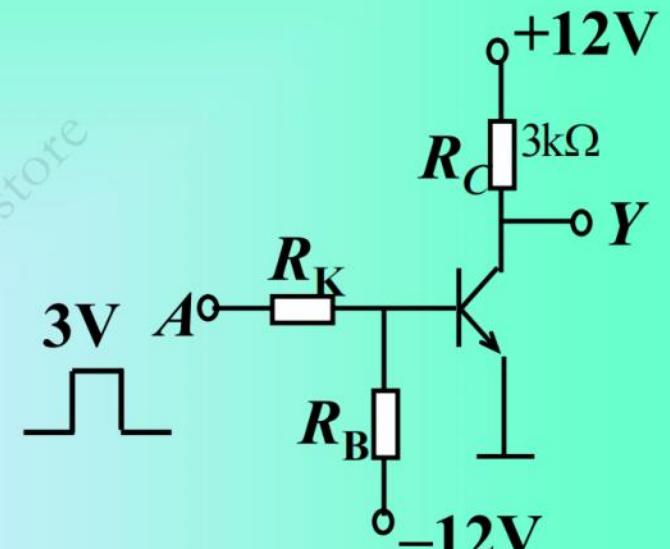
$$I_{BS} = \frac{I_{CS}}{\beta} \approx \frac{4}{\beta} \text{ mA}$$

$$I_B = \frac{V_A - V_B}{R_K} - \frac{V_B - (-12)}{R_B} = \frac{3 - 0.7}{3} - \frac{12.7}{30} = 0.34 \text{ mA}$$

$$\Rightarrow \beta \geq 12$$

$$I_B = \frac{V_A - V_B}{R_K} - \frac{V_B - (-12)}{R_B} = \frac{3 - 0.7}{R_K} - \frac{12.7}{30} = \frac{4}{30} \text{ mA}$$

$$\Rightarrow R_K \leq 4.14 \text{ k}\Omega$$



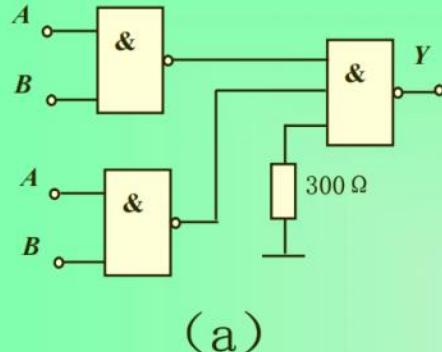
## 6.4 应用逻辑代数运算法则化简下列各式:

$$Y = \overline{\overline{AB} + A\overline{B}} = AB + \overline{AB}$$

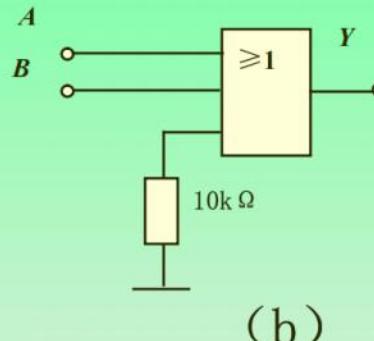
$$Y = AB + BCD + \overline{AC} + \overline{BC} = AB + BCD + \overline{ABC} = AB + C$$

$$Y = (AB + \overline{A}\overline{B} + A\overline{B})(A + B + C + ABC\overline{C}) = (A + B)(A + B + C + ABC\overline{C}) = A + B$$

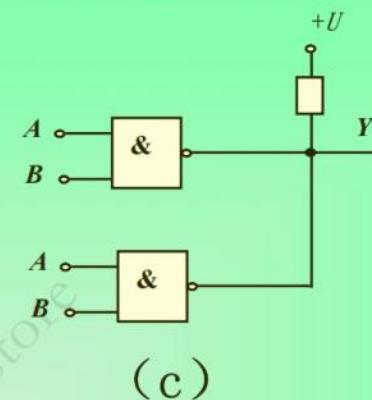
6.5 图示均为TTL门电路，试问各电路能否正常工作？并简述理由。



(a)



(b)



(c)

关门电阻 $R_{OFF}$ 及开门电阻 $R_{ON}$

$$R_{OFF} \approx 0.7k\Omega$$

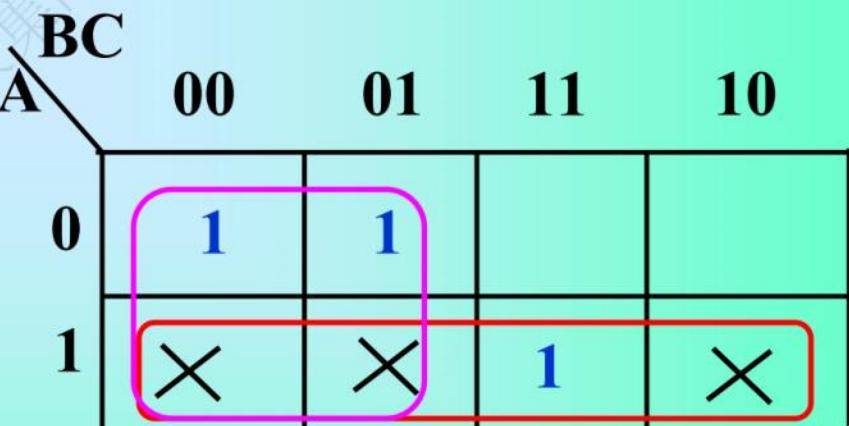
$$R_{ON} \approx 2k\Omega$$

6.6 应用卡诺图化简下列各式。

$$Y = AB + \overline{CD} + CD + ABD$$

$$= AB + \overline{CD} + CD$$

$$Y = AB + \overline{ABC} + \overline{ABC} = B$$



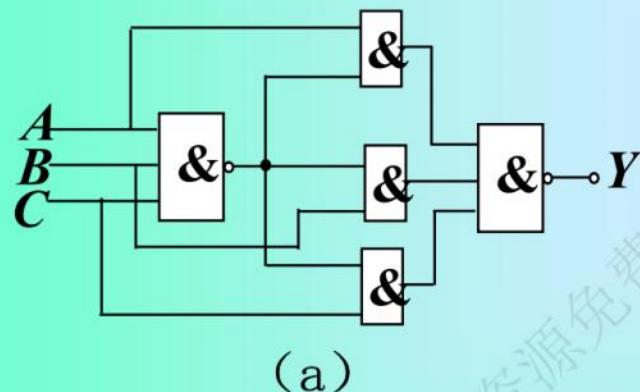
$$Y = ABC + \overline{ABC} + \overline{ABC} \quad \text{约束条件: } A\overline{B} + A\overline{C} = 0$$

$$Y = A + \overline{B}$$

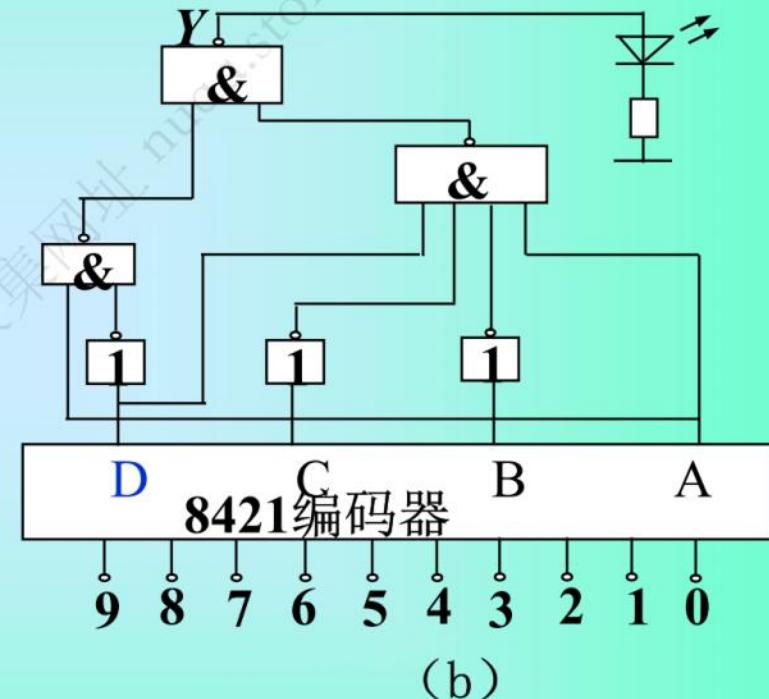
6.7 (1) 根据逻辑式  $Y=AB+\overline{A}\overline{B}$  列出逻辑状态表，说明其逻辑功能，并画出其用“与非”门组成的逻辑图。

(2) 将上式求反后得出的逻辑式具有何种逻辑功能？

6.8 分析图示电路的逻辑功能。



Y恒为1



$$Y = I_1 + I_3 + I_5 + I_7 + I_9 = \overline{\overline{I_1}} \cdot \overline{\overline{I_3}} \cdot \overline{\overline{I_5}} \cdot \overline{\overline{I_7}} \cdot \overline{\overline{I_9}}$$

输入奇数时亮灯

**6.9 在题3.10中，输出量（Q2, Q2N两个端子获得24V电压与否）与输入信号**ON, PROTECT1, SEL**之间是什么样的逻辑关系，用表达式及逻辑门电路表示。**

$$Y = \mathbf{ON} \cdot \mathbf{PROTECT1} \cdot \mathbf{SEL}$$

**6.10** 用与非门实现一个三地控制一盏灯的电路：在A、B、C共3个地方安装3个双掷开关，在任何一处拨动一次开关，灯L就会改变其亮灭状态。开关的两种位置状态分别用“0”和“1”表示，假设初始状态为：当A,B,C均为“0”时灯灭。

A	B	C	L
0	0	0	0
0	0	1	1
0	1	0	1
0	1	1	0
1	0	0	1
1	0	1	0
1	1	0	0
1	1	1	1

6.11仿照全加器设计一个一位二进制数的全减器：输入被减数为 $A$ ，减数为 $B$ ，低位来的借位数为 $C$ ，全减差为 $D$ ，向高位的借位数为 $C_1$ 。

$A$	$B$	$C$	$D$	$C_1$
0	0	0	0	0
0	0	1	1	1
0	1	0	1	1
0	1	1	0	1
1	0	0	1	0
1	0	1	0	0
1	1	0	0	0
1	1	1	1	1

7.3 已知时钟脉冲  $C$  的波形如图所示。试分别画出图中各触发器输出端  $Q$  的波形。设它们的初始状态均为“0”。指出哪个具有计数功能。

$$Q^{n+1} = J\bar{Q}^n + \bar{K}Q^n$$

$$Q_a^{n+1} = 1\bar{Q}^n + \bar{1}Q^n = \bar{Q}^n$$

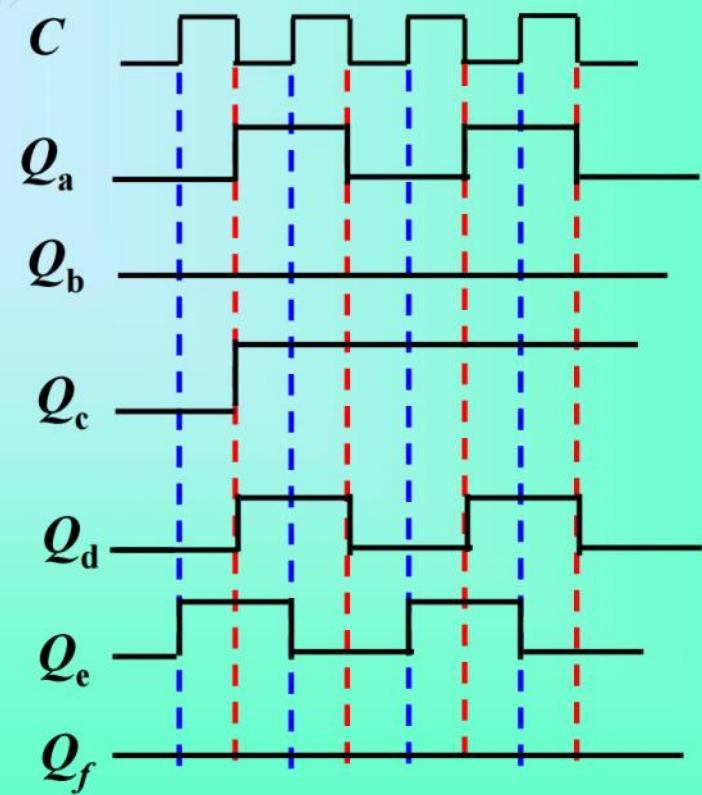
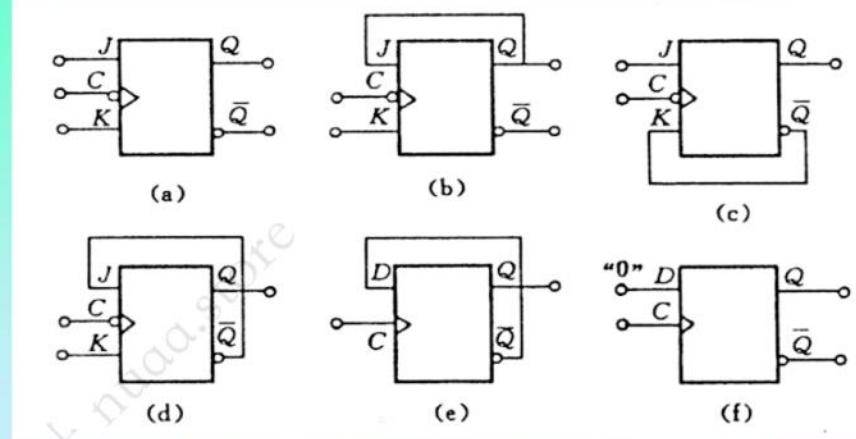
$$Q_b^{n+1} = Q^n\bar{Q}^n + \bar{1}Q^n = 0$$

$$Q_c^{n+1} = 1\bar{Q}^n + \bar{\bar{Q}}^nQ^n = 1$$

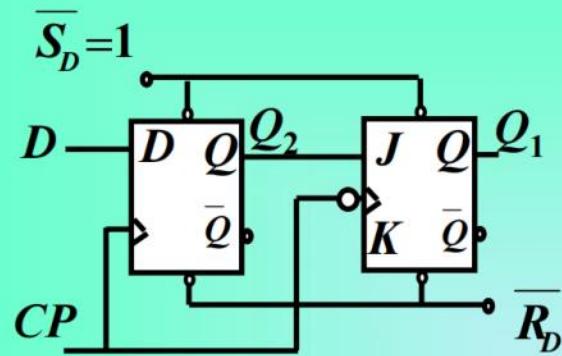
$$Q_d^{n+1} = \bar{Q}^n\bar{Q}^n + \bar{1}Q^n = \bar{Q}^n$$

$$Q_e^{n+1} = D = \bar{Q}^n$$

$$Q_f^{n+1} = D = 0$$

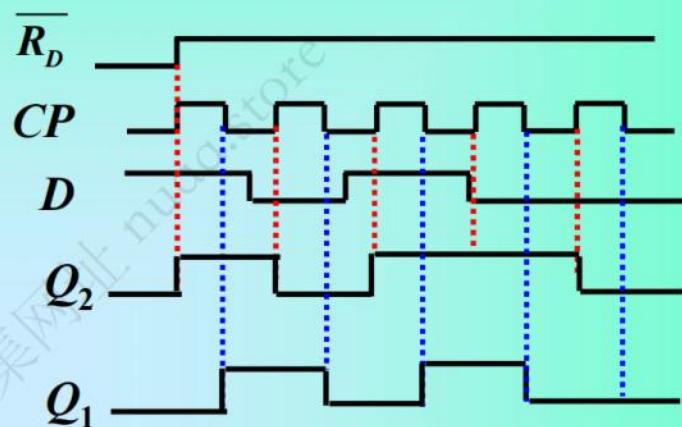


7.4 电路及信号波形如图, 请画出 $Q_2$ 、 $Q_1$ 的波形

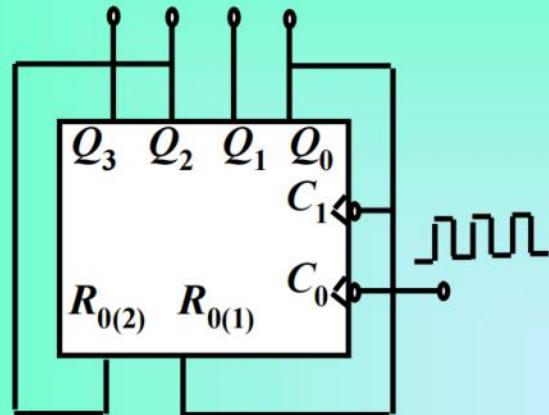


$$Q_2^{n+1} = D$$

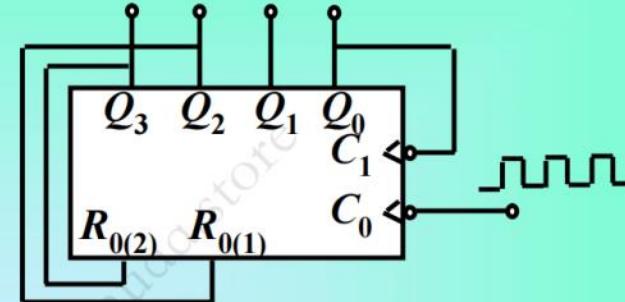
$$Q_1^{n+1} = Q_2^n \overline{Q_1^n}$$



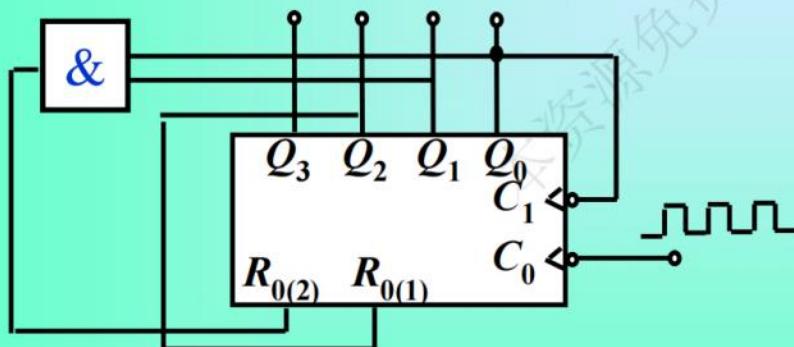
7.5 将二-八-十六进制计数器CT74LS293接成图示的两个电路时，各为几进制计数器？能否把它接成七进制或十一进制计数器。



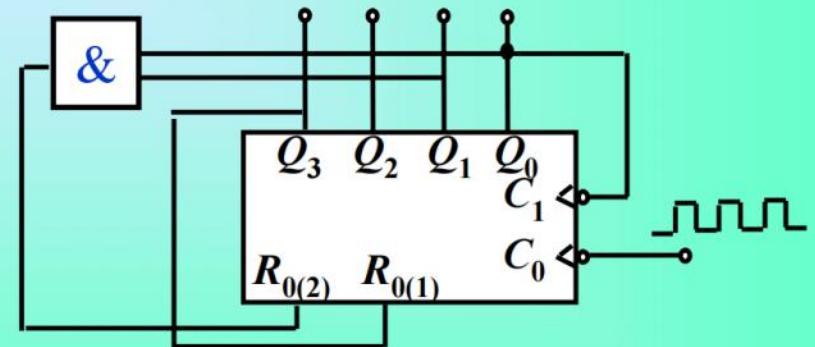
5进制



12进制

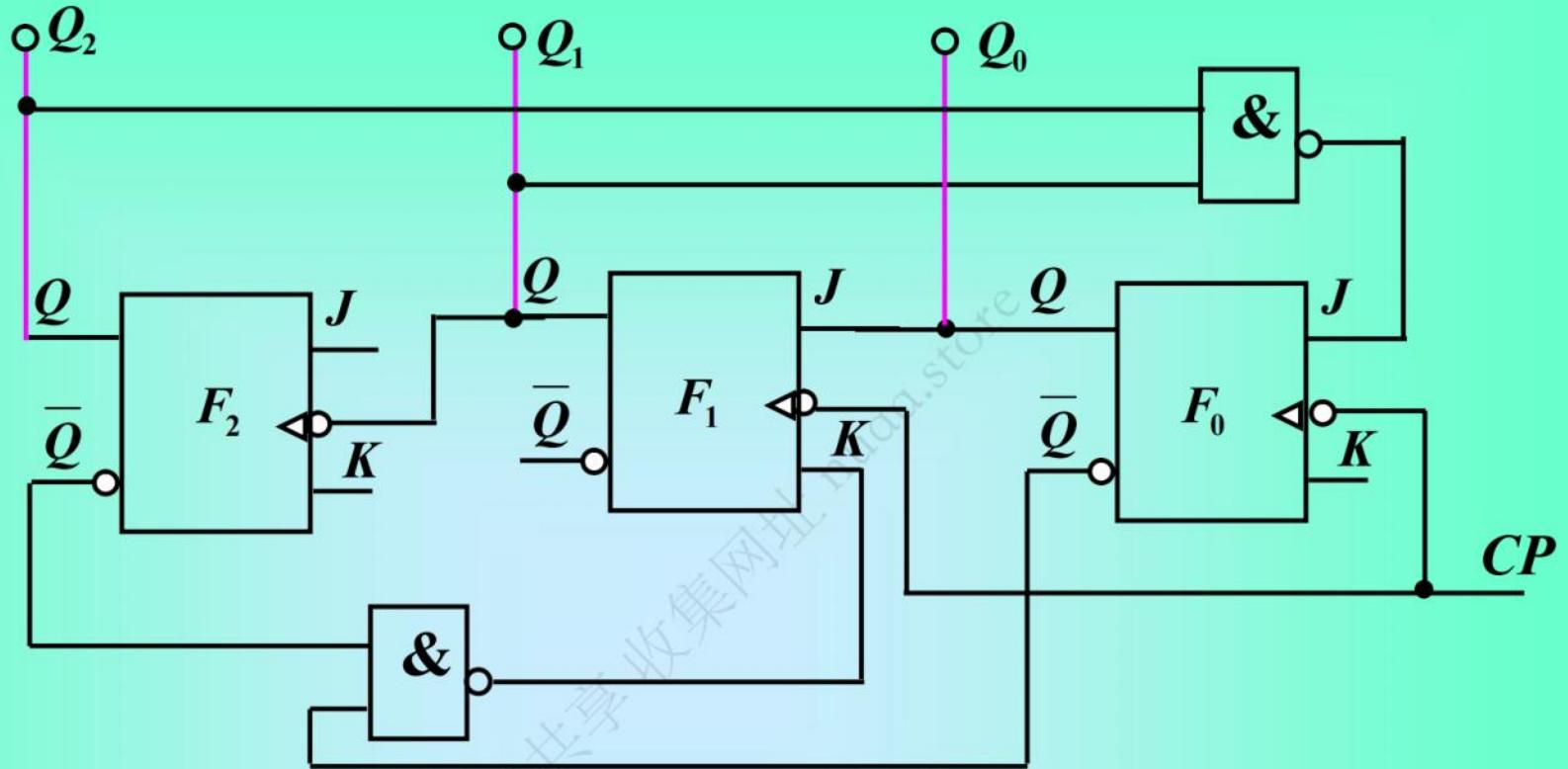


7进制



11进制

7.5



$$J_0 = \overline{Q_2^n} \overline{Q_1^n}$$

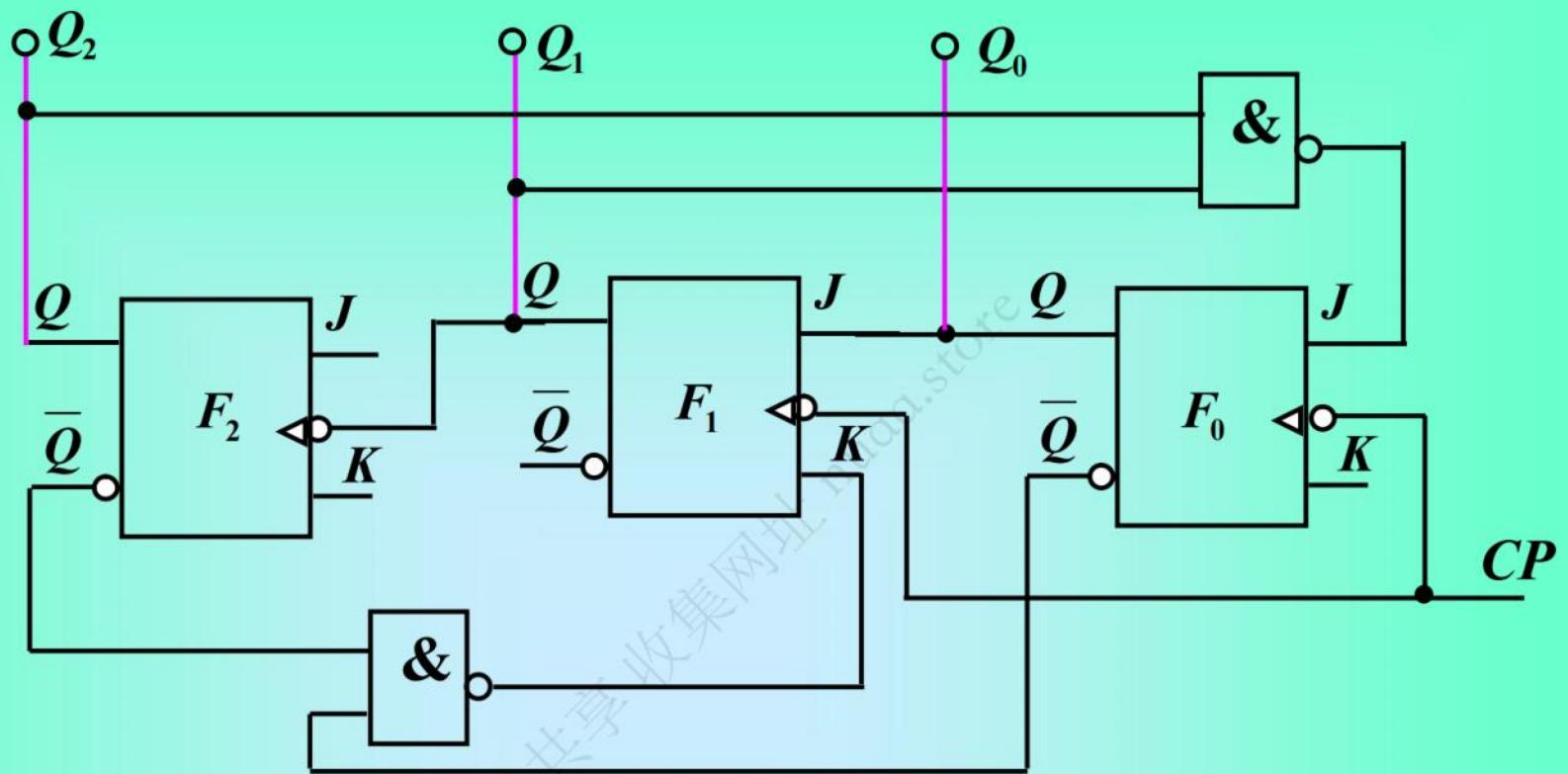
$$J_1 = Q_0^n$$

$$J_2 = 1$$

$$K_0 = 1$$

$$K_1 = \overline{\overline{Q_2^n} \overline{Q_0^n}}$$

$$K_2 = 1$$



$$J_0 = \overline{Q_2^n} \overline{Q_1^n}, \quad K_0 = 1 \Rightarrow Q_0^{n+1} = \overline{Q_2^n} \overline{Q_1^n} \cdot \overline{Q_0^n} \quad \textcolor{red}{CP} \rightarrow$$

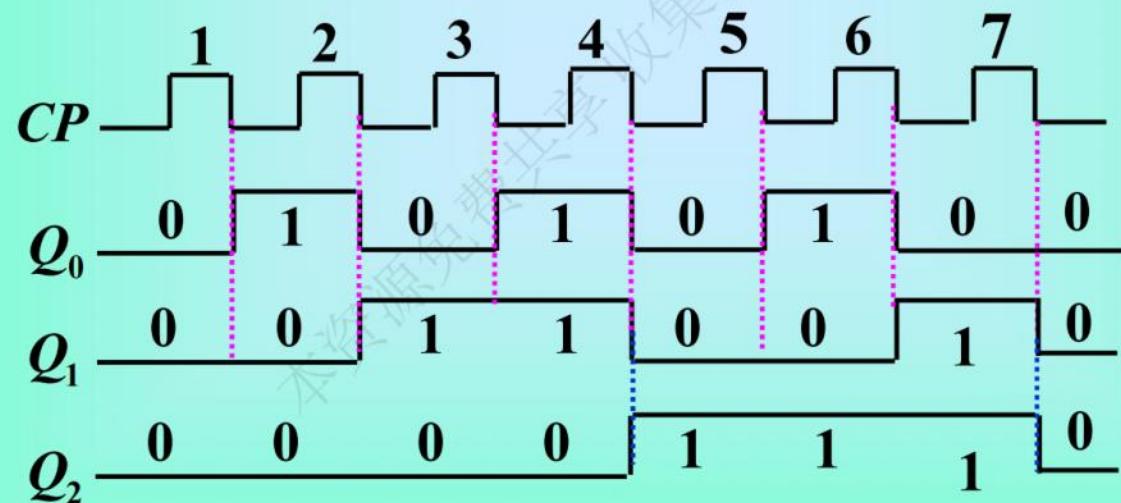
$$J_1 = Q_0^n, \quad K_1 = \overline{\overline{Q_2^n} \overline{Q_0^n}} \Rightarrow Q_1^{n+1} = Q_0^n \overline{Q_1^n} + \overline{Q_2^n} \overline{Q_0^n} Q_1^n \quad \textcolor{red}{CP} \rightarrow$$

$$J_2 = 1, \quad K_2 = 1 \Rightarrow Q_2^{n+1} = \overline{Q_2^n} \quad \textcolor{red}{Q_1} \rightarrow$$

$$Q_0^{n+1} = \overline{Q_2^n Q_1^n} \cdot \overline{Q_0^n} \quad CP \square$$

$$Q_1^{n+1} = Q_0^n \overline{Q_1^n} + \overline{Q_2^n} \overline{Q_0^n} Q_1^n \quad CP \square$$

$$Q_2^{n+1} = \overline{Q_2^n} \quad Q_1 \square$$



七进制加法计数器

$$Q_0^{n+1} = \overline{Q_2^n Q_1^n} \cdot \overline{Q_0^n} \quad CP \rightarrow$$

$$Q_1^{n+1} = Q_0^n \overline{Q_1^n} + \overline{Q_2^n} \overline{Q_0^n} Q_1^n \quad CP \rightarrow$$

$$Q_2^{n+1} = \overline{Q_2^n} \quad Q_1 \rightarrow$$

CP	$Q_2$	$Q_1$	$Q_0$
0	0	0	0
1	0	0	1
2	0	1	0
3	0	1	1
4	1	0	0
5	1	0	1
6	1	1	0
7	0	0	0

七进制加法计数器